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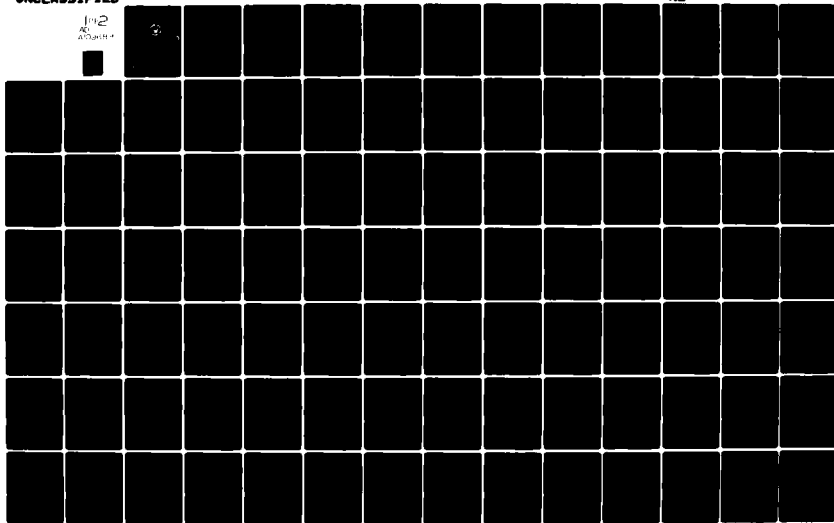
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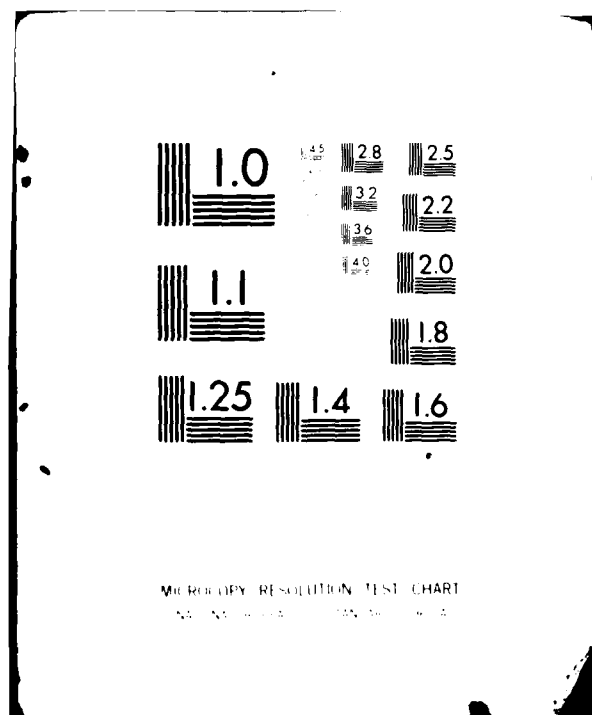
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THESIS

AN OPERATIONAL LANCHESTER-TYPE MODEL OF
SMALL-UNIT AMPHIBIOUS OPERATIONS

by

Soon Dae Park

September 1981

Thesis Advisor:

J. G. Taylor

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REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM
1. REPORT NUMBER	2. GOVT ACCESSION NO.	3. RECIPIENT'S CATALOG NUMBER
4. TITLE (and Subtitle) An Operational Lanchester-Type Model of Small-Unit Amphibious Operations	AD-A109134	5. TYPE OF REPORT & PERIOD COVERED Master's thesis; September 1981
7. AUTHOR(s) Soon Dae Park		6. PERFORMING ORG. REPORT NUMBER
9. PERFORMING ORGANIZATION NAME AND ADDRESS Naval Postgraduate School Monterey, California 93940		8. CONTRACT OR GRANT NUMBER(s)
11. CONTROLLING OFFICE NAME AND ADDRESS Naval Postgraduate School Monterey, California 93940		10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS
14. MONITORING AGENCY NAME & ADDRESS (if different from Controlling Office)		12. REPORT DATE September 1981
		13. NUMBER OF PAGES 100
		15. SECURITY CLASS. (of this report) Unclassified
		15a. DECLASSIFICATION/DOWNGRADING SCHEDULE
16. DISTRIBUTION STATEMENT (of this Report) Approved for public release; distribution unlimited.		
17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report)		
18. SUPPLEMENTARY NOTES		
19. KEY WORDS (Continue on reverse side if necessary and identify by block number) Lanchester-type combat model Amphibious operation		
20. ABSTRACT (Continue on reverse side if necessary and identify by block number) This thesis presents an operational Lanchester-type model of small-unit amphibious operations. This relatively simple model has been developed to demonstrate the basics of model building to the beginning student interested in amphibious warfare. The model is a time sequenced, deterministic, force-on-force combat model that is implemented on a digital computer. A brief discussion of considerations for modeling amphibious operations is given. The		

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An Operational Lanchester-Type Model of
Small-Unit Amphibious Operations

by

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Submitted in partial fulfillment of the
requirements for the degree of

MASTER OF SCIENCE IN OPERATIONS RESEARCH

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ABSTRACT

This thesis presents an operational Lanchester-type model of small-unit amphibious operations. This relatively simple model has been developed to demonstrate the basics of model building to the beginning student interested in amphibious warfare. The model is a time sequenced, deterministic, force-on-force combat model that is implemented on a digital computer. A brief discussion of considerations for modeling amphibious operations is given. The details of the model are presented for a specific amphibious-warfare scenario. Additionally, a computer terrain-contour-line plotting program is provided to assist the combat modeler to fit a parameterized-terrain to real terrain.

TABLE OF CONTENTS

I.	INTRODUCTION -----	7
II.	GENERAL CONSIDERATIONS FOR MODELING AMPHIBIOUS OPERATIONS -----	9
	A. CHARACTERISTICS OF AMPHIBIOUS OPERATIONS ---	9
	B. MODELING APPROACH -----	11
III.	THE MODEL -----	15
	A. GENERAL -----	15
	1. The Scenario -----	15
	2. General Description of the Model -----	16
	B. THE AMPHIBIOUS ASSAULT PHASE -----	16
	1. General -----	16
	2. Attrition Process -----	21
	3. Fire Allocation -----	25
	4. Suppression -----	28
	5. The Termination of the Assault Phase ---	30
	C. THE INITIATION OF THE GROUND ATTACK -----	30
	D. THE GROUND ATTACK PHASE -----	31
	1. Movement Process -----	31
	2. Detection and Fire Allocation -----	33
	3. Attrition -----	36
	4. Termination of Ground Attack -----	38
	E. THE PARAMETRIC TERRAIN -----	39
IV.	FINAL REMARKS -----	42
	APPENDIX A: SAMPLE EXPECTED OUTPUT -----	44
	APPENDIX B: LISTING OF SAMPLE INPUT -----	47

APPENDIX C: DEFINITION OF VARIABLE IN COMPUTER PROGRAM -----	50
APPENDIX D: PROGRAM LISTING -----	56
APPENDIX E: PLOTTING PROGRAM FOR TERRAIN CONTOUR LINE -----	96
LIST OF REFERENCES -----	99
INITIAL DISTRIBUTION LIST -----	100

I. INTRODUCTION

During the past several decades, combat models have been widely used to support military decisions. As the art of combat modeling becomes more advanced, combat modelers are continuously building more, and more complicated models. To the beginning modeler, the ability to understand how those models operate is difficult, if not impossible. It is the purpose of this thesis to develop a simple amphibious-operations model that will demonstrate the basics of model building to the beginning student interested in amphibious warfare. In the broadest sense, an amphibious operation is a combined-arms operation which includes all forms of combat--land, air, sea. This thesis will limit itself to the small-unit amphibious operation.

This project started with two basic models: one was developed as the auxiliary model for the evaluation of design and employment alternatives for the LVA (Landing Vehicle Assault) in the thesis of David Larkin Chadwick (September 1978). The other is the Smoler-Mills model which was developed in the thesis of Josef Smoler (September 1979) and enriched in the thesis of Glen Mills (September 1980).

In Chapter II, general considerations for modeling amphibious operations are briefly discussed. Then, a small-scale computer-based Lanchester-type amphibious-operations model is presented, including analytical details of the algorithms used

to represent each of the combat processes considered. Although the model was developed for a specific scenario, it is sufficiently general in design so that it can be adapted to other small-scale amphibious-operations scenarios with only relatively few modifications.

II. GENERAL CONSIDERATIONS FOR MODELING AMPHIBIOUS OPERATIONS

A. CHARACTERISTICS OF AMPHIBIOUS OPERATIONS

In order to model an amphibious operation, it is first of all necessary to understand what is going on in a real amphibious operation. Only after one knows the details of what is happening in such a complex combat operation, can one begin to sift out the cluttering details and make valid simplifying assumptions to come up with a tractable model.

One of the key characteristics that serves to distinguish amphibious operations from other types of military operations is that a complete military force must be transferred ashore in an orderly manner under the constant pressure of actual or potential attack from hostile forces. Because the over-all amphibious assault requires precise and timely execution, the various component operations must be carried out in a planned sequence (especially early in the assault) according to a strict schedule. This sequence and these schedules, however, must be sufficiently flexible to permit rapid changes in line with unexpected development afloat and ashore.

The notable success of amphibious operations during and after World War II is testimony to the fact that, with proper planning and organization, this dual problem can be solved. In today's environment, it is well known that the modern battlefield will be dominated by highly lethal weapons. This has raised serious questions about the survivability of amphibious

forces. On the other hand, the long-range, high-speed assault potentially gives one the capability to launch assaults from far out to sea, land at times and places of one's choosing, and carry more firepower to accomplish the amphibious assault with greater safety for ships and men. Use of some type of combat model is the only way to explore such issues today. In order to build such a combat model of an amphibious operation, it is necessary to develop and consider detailed and specific information on individual tactical and support elements of the landing force, on the size, numbers, and characteristics of the equipments of these elements, and on the sequence of movement of these elements.

The amphibious operation is a combined operation, the entire spectrum of activities involved in an amphibious operation includes:

- pre-assault bombardment by ships and aircraft
- sea mine clearance
- attack on ships by enemy aircraft and cruise missile
- ship-to-shore movement
- surface assault landing
- helicopter operation
- ground combat between maneuver units
- artillery and naval gunfire support
- tactical aircraft support
- mine warfare (sea and land).

While an amphibious operation is one of the most complex of all military operations, defending against it is even more

complex: it is absolutely impossible for an enemy to defend all coastal areas at all times. The flexibility to conduct helicopter-borne vertical assault and surface-borne assault simultaneously will greatly enhance the complexity of defending against an amphibious assault.

Airborne troops and supplies were valuable during the Second War, and further developments in that direction are under way. But whether or not modern airborne tactics and techniques have supplanted (in a practical sense) seaborne assaults (such as those used from 1942 through 1945 in the Pacific and elsewhere), it should be noted that the military problem of landing forces on shores held by an enemy remains. The emphasis in the future will most likely continue to be on having the ability to project forces from the sea onto a hostile shore and to hold such a beachhead.

B. MODELING APPROACH

All models of military operations must abstract from the real world. Since it is obvious that an engagement between modern military forces is a very complicated process, one has to abstract, aggregate, and interpolate in order to scale a combat process down to manageable size for modeling purposes. A variety of modeling approaches are available. These range from simple Lanchester-type models to highly complicated, computer assisted, high-resolution simulations in which the actions of each individual combatant are traced through a combat scenario second by second. Between these two extremes are

other approaches covering the whole spectrum of land combat, from one-on-one duels to theater-level models covering huge geographical dimensions.

There are basically four different types of combat models: war games, analytical (or mathematical), simulations and some combination of these first three types. According to Bonder [Ref. 2], war games are not a feasible mechanism for analyzing a broad spectrum of system alternatives in a responsive manner to meet a planning cycle requirement. However, they are diagnostic in the sense that they reveal problems that need to be resolved with future systems, and are a viable mechanism for training decision makers. Analytical models seek to describe the combat process mathematically. They simplify the conduct of sensitivity analysis and provide an increased ease in interpreting results, since the dynamics of the combat process are contained in readily examined equations. Analytical models of any degree of complexity usually do not yield convenient analytical solutions but require numerical approximation methods. Simulation is the most widely used technique in military system analysis. Simulation can generally produce very useful data, which are needed for further analysis, and sometimes for planning itself. However, the large amount of detail contained in most Monte Carlo simulations makes it difficult to use as the sole vehicle to single out those systems capabilities, tactics, and environmental conditions which significantly contribute to or delimit the system's effectiveness. Since, as we have seen above, no one type of combat model

is unconditionally preferred to another, it is proposed that a combat model should be selected or designed based on a specific scenario and upon analytical requirements.

In most cases, detailed models are more credible to decision makers. However, for many people such detailed models of large-scale combat operations are far too complicated to be understood, require too much input data, and (in general) are not responsive enough. When one looks at computer storage and run time requirements for even the smallest high resolution model, it is easy to see why a high resolution model of a corps or theater is presently impractical, and is likely to remain so. In order to avoid the complexity of the large-scale model and to better understand land combat there is a growing trend among analysts to combine small unit and large unit models in such a way that the output data of a high-resolution small unit combat model is used as the input data for a low-resolution large unit model. The obvious drawback of this hierarchical-modeling approach is that any errors in the small unit models will be carried through, and possibly multiplied, as the process proceeds from model to model. In the large units the emphasis has been away from simulation and towards detailed Lanchester-based models.

So far the emphasis has been adding more and more detail to the high resolution models so as to pick up as many interactions as possible. No matter how much detail is added to the small-unit simulation, it seems impossible that reality will ever be matched exactly. With this in mind, it is proposed

that a well-constructed Lanchester-based model of small unit engagements could give results that are just as valid as the results of a high-resolution simulation.

III. THE MODEL

A. GENERAL

1. The Scenario

The scenario considers an amphibious-landing team, consisting of reconnaissance, a light infantry unit, and landing-assault vehicles. This team is part of an Amphibious Task Force (ATF), and it disembarks from ships that are on station over the horizon from the selected landing site. The assault vehicles, after transmitting from the amphibious shipping to the designated area for the landing formation, form into conventional landing waves at a distance offshore which is greater than the effective range of the direct-fire weapon systems of the shore-defense force. During the ship-to-shore movement the defender's anti-tank guided missile and improved gunnery system respond to the landing. Naval gun-fire ships provide fire support for the assault team during the ship-to-shore movement and the initial stages of landing.

As the assault vehicles reach the beach, they (together with the assault vehicles and any weapons landed by landing vehicles) launch an attack on the enemy shore defense positions. The defenders occupying those positions fight until their losses exceed a maximum permissible amount. The attacking force, however, continues the assault irregardless of losses incurred. Once the shore assault has been completed, the landing force with tactical mobility moves inland to

carry out the tasks, while the enemy prepares to mount a counter attack.

The attacker may engage the advance force of the defender's initial counter attack force on the way to move inland. The advantage will likely go to that force which has gained the initiative (i.e., the landing force) provided it can maintain its momentum.

2. General Description of the Model

The model developed in this thesis is a time sequenced, deterministic, force-on-force computerized model, coded in FORTRAN. The model conducts the battle in uniform time steps of 10 seconds each. Figure 1 shows the general scheme for the sequence of events in the model. The model simulates two main phases in the amphibious operations: (I) the amphibious-assault phase, and (II) the subsequent ground attack. The framework and the logical interrelationships of these two phases will be discussed in the following subsections.

B. THE AMPHIBIOUS ASSAULT PHASE

1. General

In this phase the model considers attrition between the shore-defense force and the landing-assault force during its water-borne movement and subsequent assault to shore. The model aggregates the various actual combat organizations involved in the waterborne phase of the amphibious operation into several homogeneous combat units. Each of these units is characterized by certain relative offensive and defensive

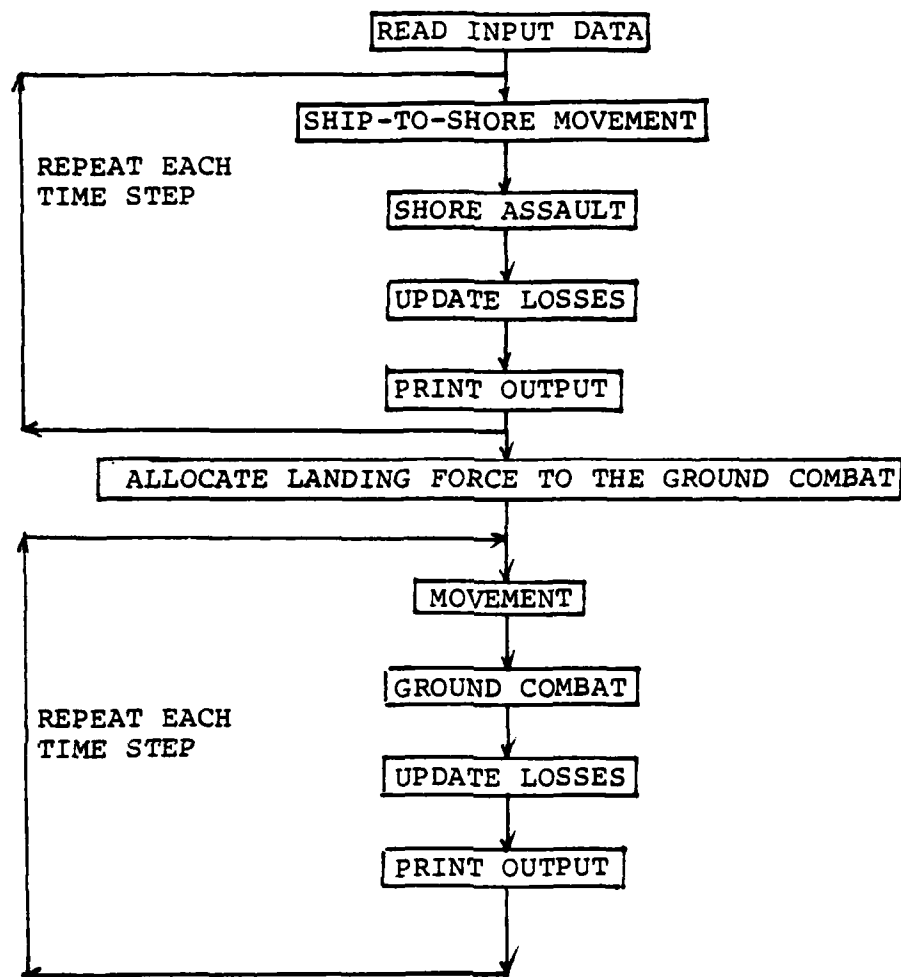


Figure 1. General Scheme for the Amphibious Operation Model

capabilities. The following table illustrates the combat organizations that were explicitly modeled. The combat strength of each unit was represented by the state variables indicated.

<u>combat organization</u>	<u>state variable</u>
Shore Defense--TANK assets	DT
Shore Defense--ATGM assets	DS
Incoming assault waves of LVA representing waves 1 through 5	WV(I), I = 1,2,3,4,5
A cumulative combat force comprised of those Marine ground units which have arrived at the beach and have debarked the LVA	TLF
Fire Support Assets of The Amphibious Task Force	ATFFS

The initial strength in each of the above units is input data to the model.

The schematic of the method of employment for the LVA in the ship-to-shore phase of an amphibious assault is shown in Figure 2. It is assumed that the conventional landing formation composed of waves of landing vehicles will be used as prescribed by current doctrine. The movement of assault vehicles to the beach is simulated using a time step approach. At each time increment the positions of vehicles are updated.

The tactical interrelationships which exist between various combat units are illustrated in Figure 3. Assuming that in such a future amphibious operation the attrition of

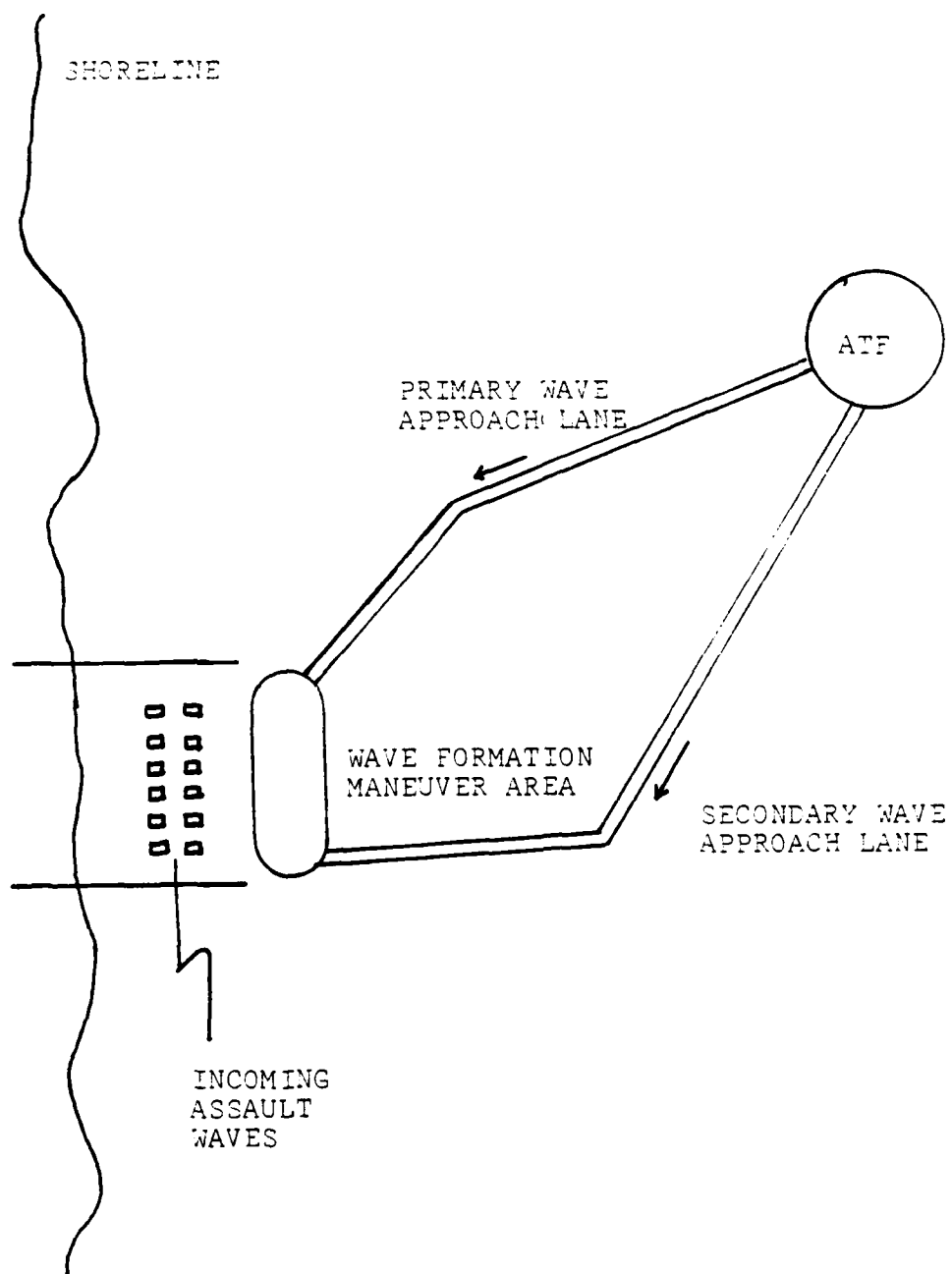


Figure 2. Concept of Ship to Shore Movement

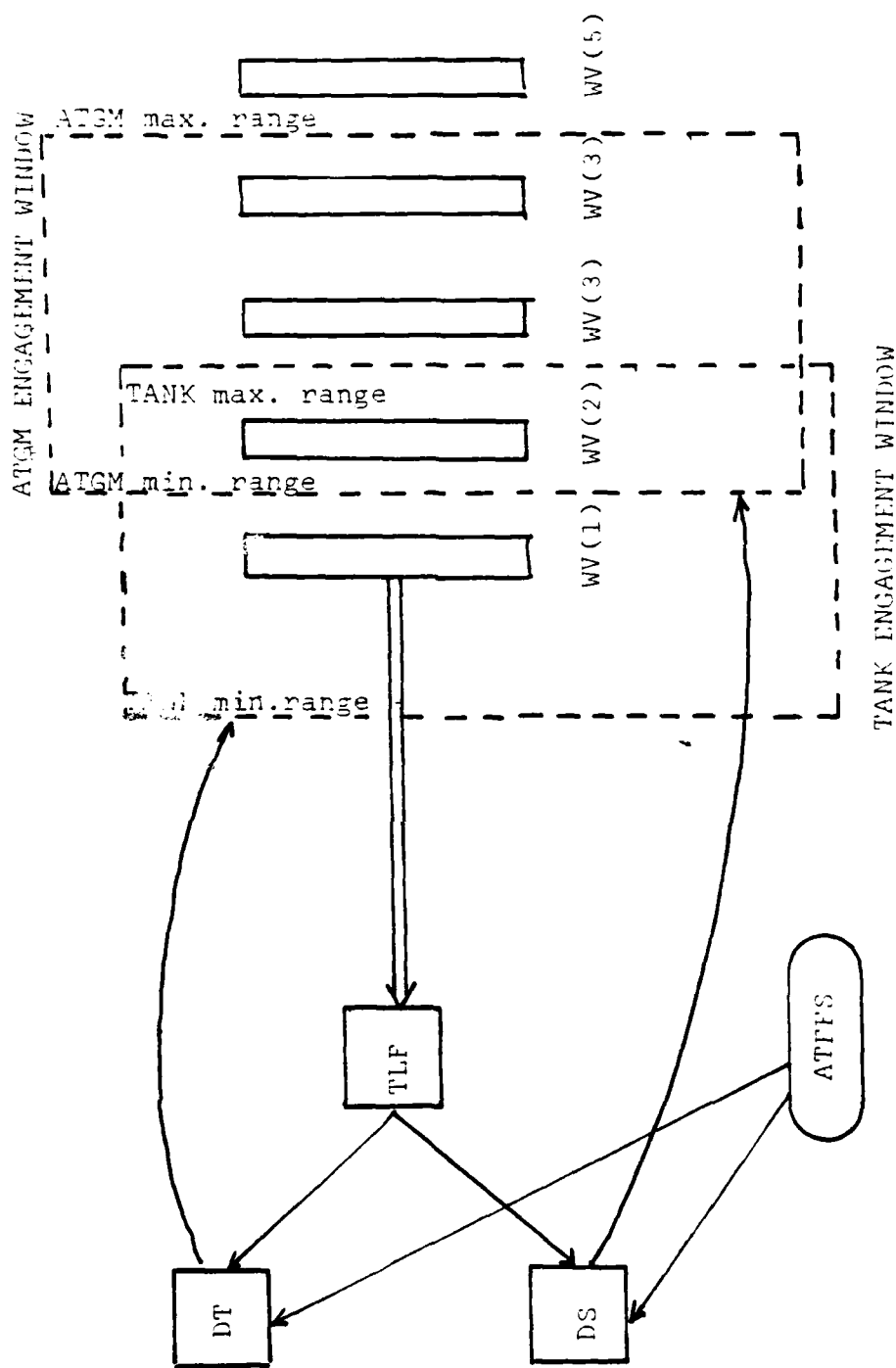


Figure 3. Schematic of Tactical Interrelationship between Combat Units during Amphibious Assault Phase

incoming landing vehicles would be dominated by the effects of shore defense direct-fire weapon systems (specifically, tank and anti-tank guided missile (ATGM) assets), the model essentially omits the effect of the defensive indirect fire capabilities.

2. Attrition Process

The model represents the attrition of all combatant units as a deterministic process. The primary consideration in the ship-to-shore movement of incoming waves of assault vehicle is the attrition effects upon those waves due to the direct fire weapon assets ashore. The attrition of each wave utilizes Lanchester "aimed-fire" equations with variable attrition-rate coefficients.

The classical Lanchester hypothesis for aimed-fire attrition (combat under "modern condition") is that the casualty rate of a unit is proportional to the "size" of the opposing forces. If the unit "A" is being engaged by "D", this may be expressed by the differential equation:

$$\frac{dA}{dt} = - \text{BETA}_{DA} \times D$$

The proportionality constant BETA_{DA} is called the Lanchester attrition-rate coefficient. It is assumed that this functional relationship holds for each (firing unit, target unit) pairing over a small time interval dt . The problem then is to determine numerical values for the Lanchester attrition-rate coefficients. In this model, these coefficients were expressed

as the product of the rate of fire (ROF) and the kill probability per round (P_k). Thus,

$$BETA_{DA} = ROF_{DA} \times P(k)_{DA}$$

The rate of fire (ROF) can be expressed as the reciprocal of TBF (Time Between Firings) which can be evaluated by

$$TBF = AIM-RELOAD TIME + \frac{TARGET RANGE}{TARGET SPEED + PROJECTIVE VELOCITY}$$

In determining the probability of a vehicle "KILL" per round, it is assumed that a hit by a large caliber projectile would constitute a "KILL" and the two defensive weapon systems addressed would exhibit normal, uncorrelated horizontal and vertical errors. Then the single shot kill probability is given by

$$P(k) = \left[\left(\frac{1}{\sqrt{2\pi}} \right) \int_{(-a-u)/\sigma_x}^{a-u/\sigma_x} \exp\left(-\frac{x^2}{2}\right) dx \right] \cdot \left[\left(\frac{1}{\sqrt{2\pi}} \right) \int_{(-b-v)/\sigma_y}^{(b-v)/\sigma_y} \exp\left(-\frac{y^2}{2}\right) dy \right]$$

where:

- a = semilength of a target
- b = semiwidth of a target
- u = horizontal aiming error
- v = vertical aiming error

σ_x = round-to-round standard deviation in vertical

σ_y = round-tround standard deviation in horizontal

Model functions RNG, HT and SPD are called upon within the model logic to generate the range, height and speed respectively for each assault wave as time is incremented throughout the course of the amphibious assault phase. This information and typical dispersion data (both mean and standard deviation for the tank and ATGM weapons) are then incorporated into the rate of fire and hit probability calculations.

The Amphibious Task Force's fire support assets contribute significantly to the combat effectiveness of the shore defense units. Since it is assumed that the exact positions of the defensive units DT and DS emplaced on shore are unknown to the Amphibious Task Force and consequently the ATF fires into the general areas thought to contain the defensive units. The following Lanchester-type area-fire equations are applied to compute the attrition of DT and DS.

$$\frac{dDT}{dt} = -(\text{ALPHA}_{DT} \times \text{ATFFS}) \times DT$$

$$\frac{dDS}{dt} = -(\text{ALPHA}_{DS} \times \text{ATFFS}) \times DS$$

The combat effectiveness of the ATF fire support assets is to be considered relatively constant during this segment of combat time. Thus the terms in parentheses on the right hand side of these equations are to be considered an input parameter.

Once a particular defensive unit has initiated its engagement of incoming waves it is considered that their fire "gives away" their exact locations. At this point it is assumed that the ATF fires will engage that defensive unit through the use of aimed-fire and the loss rate will be in accordance with the Lanchester hypothesis for aimed fire. That is,

$$\frac{dDT}{dt} = -\text{BETA}_{DT} \times \text{ATFFS}$$

$$\frac{dDS}{dt} = -\text{BETA}_{DS} \times \text{ATFFS}$$

Again, the parameters on the right-hand sides of both these equations are provided as input.

The casualty rates applied against the DT and DS by the Total Landed Force (TLF) are determined by means of the Lanchester aimed-fire attrition rate coefficients by the equations

$$\frac{dDT}{dt} = -\text{WBETA}_{\text{TLF-DT}} \times \text{TLF}_{DT}$$

$$\frac{dDS}{dt} = -\text{WBETA}_{\text{TLF-DS}} \times \text{TLF}_{DS}$$

The computation of these WBETA coefficients is not performed within the model utilizing the detailed rate of fire and $P(k)$ arguments described previously but is required as input. Although the defensive losses are considered significant,

a high level of complexity for computing these coefficients has not been incorporated into the model at this time.

Figure 4 describes the schematic of the attrition process of the amphibious assault phase in the model. The attrition during each time step was computed using the Euler integration method to approximate Lanchester's force-on-force attrition differential equations.

3. Fire Allocation

Each weapon category was assigned an engagement window as illustrated in Figure 3. Only those LVA located within these range windows could be fired upon by the shore defenders. A defensive weapon only engages the two closest incoming waves if more than two waves of LVA are at any time located within the weapon's engagement window. If only one wave of LVA is present in a weapon's engagement window, defensive fires of that particular weapon type will be distributed uniformly against the surviving LVA in that wave.

If two waves of LVA are both contained within the engagement window, defensive fires of that particular weapon type will be distributed according to a tactical allocation submodel. A weighting factor (DEFWT) is utilized in establishing the proportion of the total weapon strength to be allocated against the surviving LVAs in each of the two waves. As an example, if $DEFWT(1) = 2$ and $DEFWT(2) = 1$, then each surviving LVA in the closer of the two incoming waves would be allocated twice as much fire as surviving LVA in the seaward

DIRECT FIRE DT/DS AGAINST FOR EACH INCOMING WAVE I

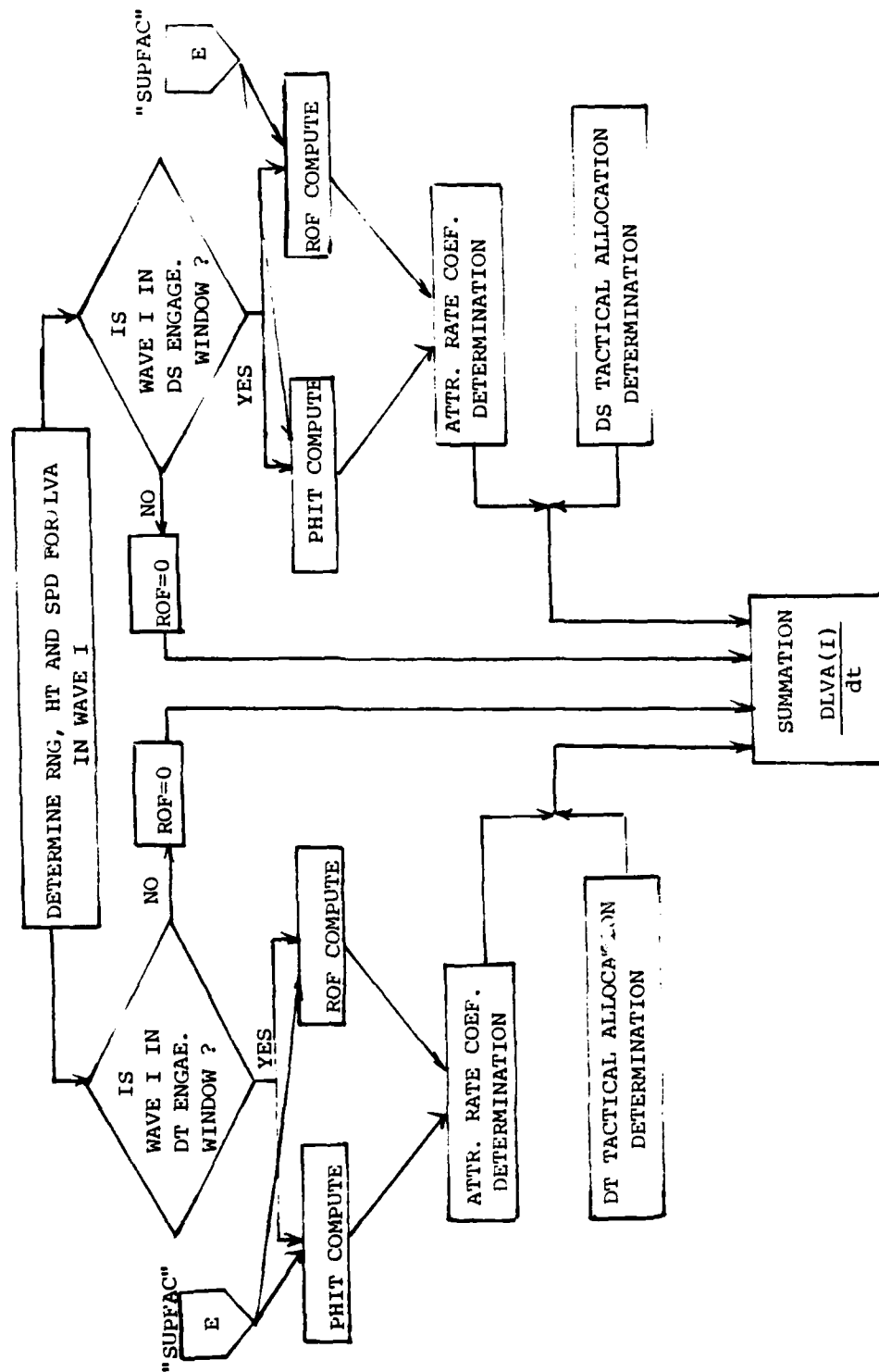


Figure 4. Schematic of The Attrition Process for The Assault Phase

ATTRITION FOR THE SHORE DEFENSE FORCE

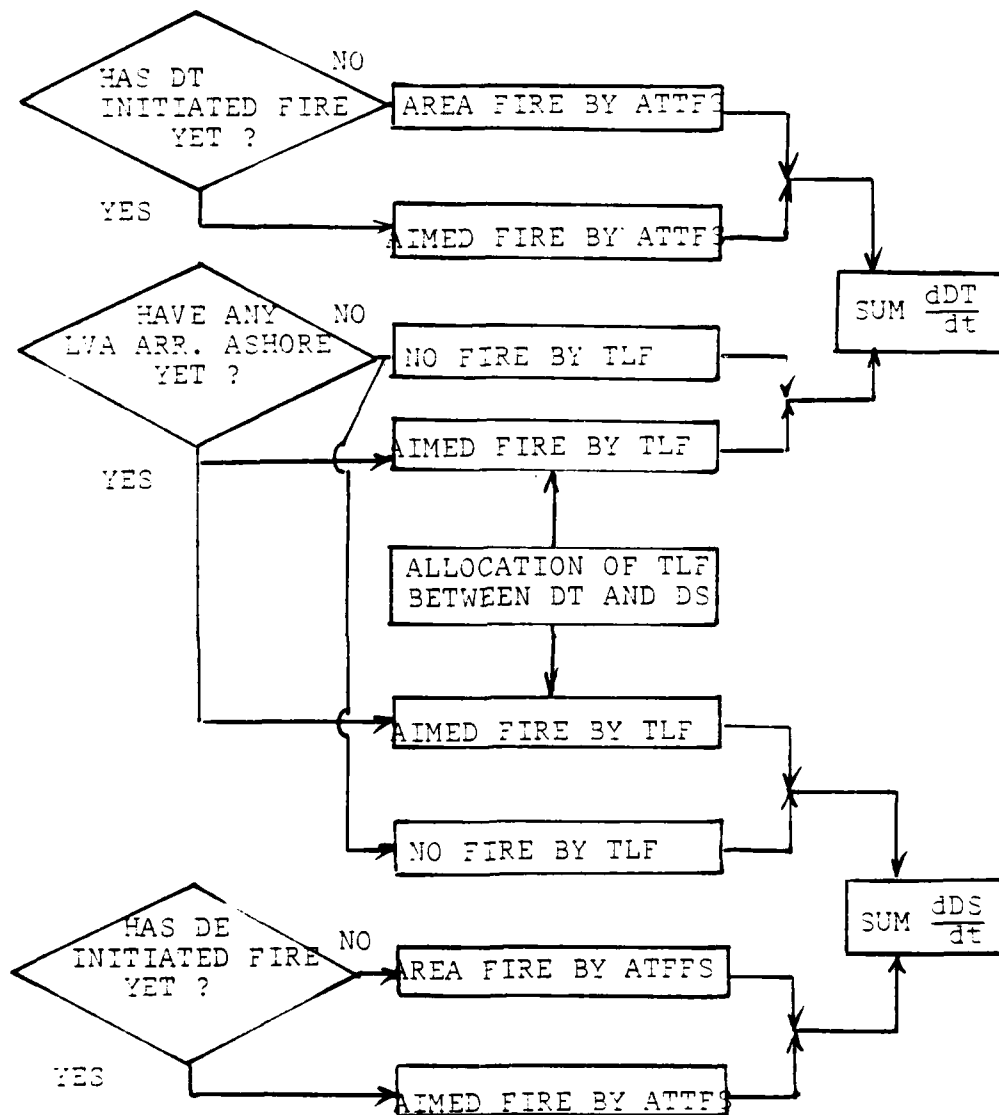


Figure 4.(cont)

wave. For the purpose of these examples, if waves 3 and 4 were both located within the tank engagement window, then the proportion of DT's fire allocated to surviving LVA in wave 3 would be

$$\frac{\text{DEFWT}(1) \times \text{WV}(3)}{\text{DEFWT}(1) \times \text{WV}(3) + \text{DEFWT}(2) \times \text{WV}(4)} \times \text{DT}$$

where WV(3) is the state variable for the current number of survivors in wave 3.

As each assault wave arrives at the beach, the total surviving strength of that wave is transferred to the variable TLF (Total Landed Force). TLF represents a ground combat force equal to that transported by the number of LVA survivors having arrived ashore. Once established, TLF engages the two shore defensive units allocating its fires between the two defensive weapon categories in the same proportion as the number of surviving tanks and ATGM's, that is

$$\text{TLF}_{\text{DS}} = \frac{\text{DS}}{\text{DT} + \text{DS}} \times \text{TLF}$$

$$\text{TLF}_{\text{DT}} = \frac{\text{DT}}{\text{DT} + \text{DS}} \times \text{TLF}$$

4. Suppression

The suppression effects of incoming fire upon each of the defensive units was considered a significant factor with respect to its effect on the survivability of the incoming assault waves of LVA. Generally, the effect of suppression

fire will hinder an individual from observing and firing at the enemy.

It was assumed that suppression would degrade unit effectiveness by increasing the aim-reload time (ARTM) and round-to-round error standard deviation for each weapon system. Hypothesizing that attrition rate is the dominating variable, and therefore, a good indicator of the suppression level, ARTM and such round-to-round errors were assumed to be functions of the force's attrition rate. This is an area, however, requiring further study. Analytically,

$$ARTM_{sup} = ARTM_{nonsup}(1 + GAMMA \times DA)$$

$$ERROR_{sup} = ERROR_{nonsup}(1 + DELTA \times DA)$$

where:

- DA = attrition rate for defensive unit due to the effect of AFTTS and TLF
- GAMMA = parameter representing relationship between DA and ARTM
- DELTA = parameter representing relationship between DA and error standard deviation

This increase of ARTM and round-to-round error (expressed as a standard deviation) decreases the kill probability (P_k) for both defensive weapon categories. Parameter estimation would appear to be the largest problem. But, since determining these parameters in the model is beyond the scope of this thesis, these parameters GAMMA, DELTA are provided as input.

5. The Termination of the Assault Phase

It is assumed that if during the course of the amphibious operation the shore defense forces suffer a cumulative loss in excess of 70% of their initial force strength, the remaining shore defense will try to withdraw, resulting in termination of the engagement.

C. THE INITIATION OF GROUND ATTACK

In the amphibious operation, the landing-force must seize critically-important inland objectives as rapidly as possible before the defenders start to react to the landing. The decision for the initiation of ground attack should be based upon the enemy threat and desired landing-force build-up ashore, among other factors. To model this decision rule, it is assumed that once the landing has begun, the landing-force commander will base his decision about initiation of ground attack primarily on the strength of the landing-force ashore and the shore defender's strength. The criteria for the decision should meet these two conditions:

- (1) The survived landing-force strength has to be greater than the minimum force required to carry out the ground attack.
- (2) The defender's strength must fall below the minimum required to continue coordinated shore defense before breakoff and retreating.

These conditions are then checked after each time step. If all waves landed without reaching the above second conditions, it

is assumed that the next wave group will engage any leftover defenders. Thus, the decision to implement the ground attack is based on the size of the total landed force.

D. THE GROUND ATTACK PHASE

The attacking force which is composed of three subunits of three LVAs armed with TOW antitank missile system attacks along predetermined routes. The defending force is comprised of three subunits of three tanks in a static defense.

The battle takes place on parameterized terrain which will be discussed later. The ground-attack process contains five main subprocesses: (1) movement, (2) detection, (3) fire-allocation, (4) attrition and (5) battle termination. The general flow of the ground attack phase is shown in Figure 5.

1. Movement Process

Every attack unit is advanced to the next interval along a predetermined route unless this unit is destroyed already or is in firing status. To use his own determined routes, the user is required to input the original location of each attacking subunit and from one to ten nodes he wishes each attacking subunit to move through. This information, along with vehicle speed, is used to calculate route intervals that move the attacking unit through each of the designated nodes. The straight line ground distance between the first two adjacent nodes, DIST, is calculated as

$$\text{DIST} = \sqrt{X^2 + Y^2}$$

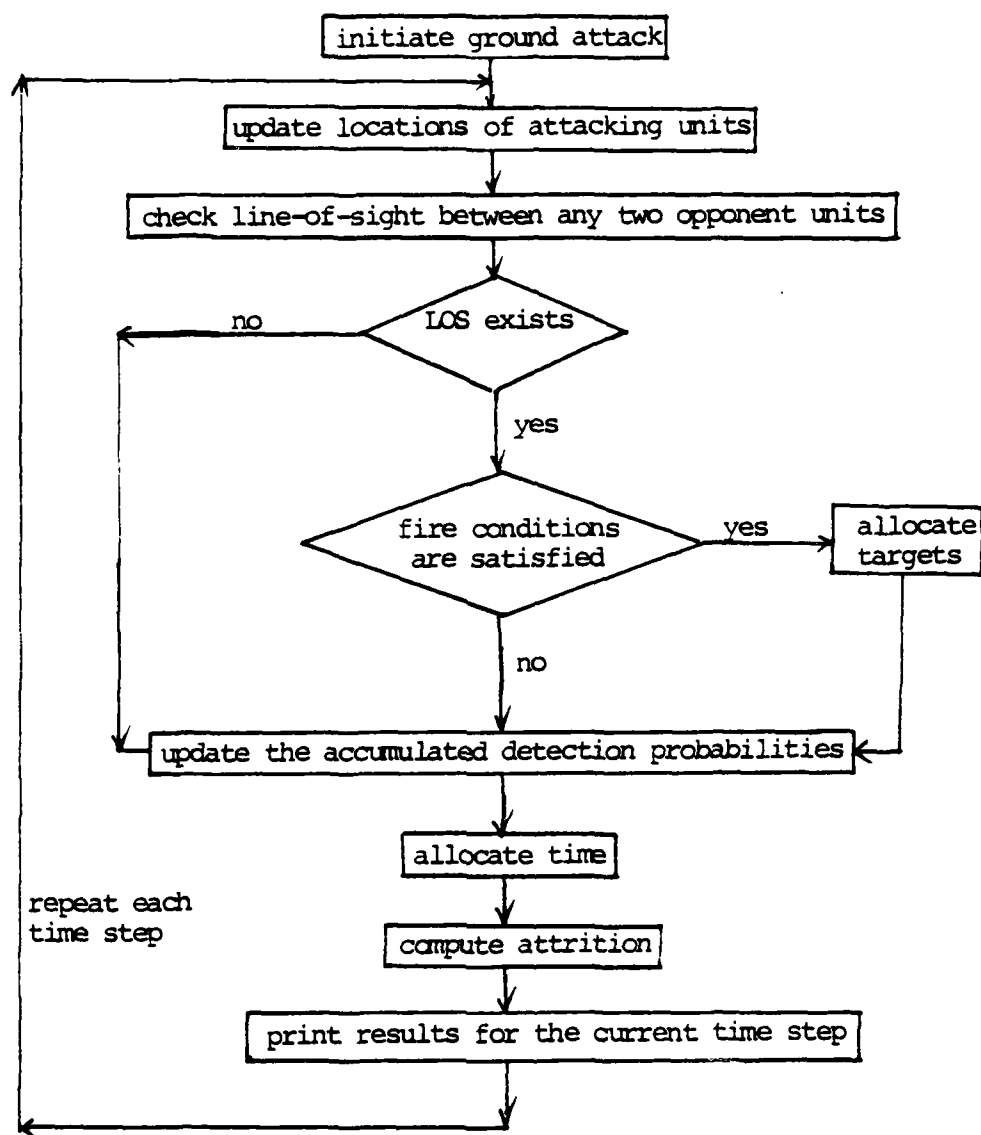


Figure 5. Flow Chart for the Ground Attack Phase

where:

X = distance between two nodes in straight west-east direction

Y = distance between two nodes in straight south to north direction

The angle between the desired direction of movement and straight west to east movement, α , is then calculated. Utilizing these quantities, the distance desired to move during each time step (DST) and the distance to be moved in the X and Y direction (XLN, YLN) is computed. These distances (XLN, YLN) are then added to the coordinates of the previous interval endpoint to determine the coordinates of the next interval endpoint. This process is repeated between the next two nodes until the unit has traversed the entire route.

2. Detection and Fire Allocation

The detection phenomena are modeled in two ways:

(I) non-firing detection, and (II) firing-detection. A non-firing detection can occur as a result of an observer's random search within his designated sector of responsibility. The probability (P_k) that an observer A looking at the direction which enables him to detect a target is computed by integrating the Limicon Function over limits are $\pm 15^\circ$ from the primary direction the observer is looking. The Limicon Function, $f(\theta)$, is the following probability density function:

$$f(\theta) = A + B \times \cos(\theta) \quad -0 \leq \theta \leq 0$$

where:

$$\begin{aligned} D &= \text{assigned sector width}/2 \\ A &= -B \times \cos(D) \\ B &= \frac{1}{2}(\sin(D) - D \times \cos(D)) \\ \theta &= \text{primary direction observer is looking} \end{aligned}$$

Assuming 30° field of view for any observer A target B might be seen only if the observer A is looking at the direction such that $\text{ANGRT} \leq \theta \leq \text{ANGLFT}$ where:

$$\begin{aligned} \text{ANGLE} &= \text{the absolute value of the angle between the primary direction (IPRDIR) and the observer-target direction (OTANG)} \\ \text{ANGLFT} &= \begin{aligned} &\text{angle} + 15^\circ \text{ if } \text{angle} + 15 \leq D \\ &D \text{ if } \text{angle} + 15 > D \end{aligned} \\ \text{ANGRT} &= \text{angle} - 15^\circ \end{aligned}$$

Thus

$$\begin{aligned} P_k &= \text{pr}(\text{ANGRT} \leq \alpha \leq \text{ANGLFT}) \\ &= \int_{\text{ANGRT}}^{\text{ANGLFT}} f(\alpha) d\alpha \end{aligned}$$

Given that observer A is looking at the direction, the conditional detection rate (λ_{AB}) is determined by the regression curve [Ref. 11]. The probability that unit j is detected by unit i at time $t + \Delta t$ [$P_{ij}(t + \Delta t)$] is computed according to:

$$P_{ij}(t + \Delta t) = 1 - e^{-\int_t^{t+\Delta t} \lambda(t) dt}$$

$P_{ij}(t)$ can be interpreted as the average fraction of unit i that detects unit j .

The second method of detection played in the model is a so-called firing detection. This phenomena occurs when the following happens: if a firing location is within $\pm 15^\circ$ of an observer's primary direction of observation when he is firing, he is assumed to be detected and is added to the observer's target list. In summary, the following conditions are necessary for unit j to be a target of unit i :

- (a) Line-of-sight must exist between unit i and unit j .
- (b) The range between the two units should be between maximum range and minimum range of the firer's weapon system.
- (c) $P_{ij}(t - \Delta t) > 0$.

The fire-allocation routine determines what fraction of each unit is allocated to fire each target in target list since it is assumed that each fire unit is not restricted to fire at one target. This fraction is determined as a function of the predetermined fire policy and $P_{ij}(t)$. The fire policy is as follows:

# of target	% of unit i allocated to each target		
	1 st priority	2 nd priority	3 rd priority
1	100%		
2	80%	20%	
3	80%	15%	5%

The priority of a target is taken to be a function of range only. The fire allocation rule which is used in the model is documented in detail in Smoller's thesis [Ref. 9].

3. Attrition

The attrition process in the ground attack phase utilizes Lanchester "aimed-fire" equation used with variable attrition coefficients. The calculation of the attrition coefficients is accomplished through the use of one of two optional methods. The first option uses the following Bonder-Farrell formula to compute the reciprocal of the expected time to kill. The coefficients, A_{ij} , the rate at which one firer of unit i kills unit j targets are computed according to:

$$A_{ij} = 1/E(T_{ij})$$

where $E(T_{ij})$ is the expected time for one firer of unit i to kill one target of unit j . The $E(T_{ij})$ is computed using:

$$\begin{aligned} E(T_{ij}) = & t_a + t_1 - t_h + (t_h + t_f)/P(K/H) \\ & + (t_m + t_f)/P(h/m) \times ((1-P(h/h))/P(K/H) \\ & + P(h/h) - p) \end{aligned}$$

where:

t_a = time to acquire a target

t_1 = time to fire first round following acquisition

t_h = time to fire following a hit
 t_m = time to fire following a miss
 t_f = time of flight of a round
 P = probability of a first round hit
 $P(h/h)$ = probability of a hit following a hit
 $P(h/m)$ = probability of a hit following a miss
 $P(k/h)$ = probability of a kill given a hit

This formula holds for the conditions that the hit probability of any round depends only on the result of the previous round and no accumulated damage is considered. It is assumed that $P(K/H) = 1.0$ and $P(h/m) = p(h/h) = P$, thus reducing the equation to:

$$E(T_{ij}) = t_a + t_l + t_f + (t_m + t_f)(1-P)/P$$

The second method, called the stochastic method, interprets the attrition rate coefficient, A_{ij}^0 , as a measure of the fighting ability of a unit which has a random phenomena affected by many different factors. It is assumed that the random fighting ability should be distributed between .3 and .8 with the majority of the unit being rated between .5 and .6. A "fitted" distribution to these assumed fighting levels which is devised by Mills is:

$$A_{ij}^0 = -2U^2 + 2U + .3 ; \quad U \text{ is a random Uniform } (0,1) \text{ number}$$

The A_{ij}^0 's are a realization of the random variable denoting a unit's initial fighting capability prior to the battle. Then,

during each time step, a new attrition rate coefficient for each unit is computed using the equation:

$$A_{ij} = \begin{cases} A_{ij}^0 (1 - r/r_e) & ; \text{ for } 0 \leq r \leq r_e \\ 0 & \text{ for } r_e \leq r \end{cases}$$

where:

r_e = maximum effective range of a firer's weapon
 r = current range between firer and target

Utilizing one of the above formulas to calculate A_{ij} 's, the attrition during each time step was computed using the Euler-Cauchy differencing equations to approximate Lanchester's force-on-force attrition differential equations.

4. Termination of Ground Attack

The ground attack is terminated when either:

- (1) One of the two opponent forces is annihilated;
- (2) A distance between each attacking subunit and each defensive subunit which is still engaging becomes "too close";
- (3) Any attacking subunit passes by the flanks of the forward most defensive subunit still in the battle.

The criteria for being "too close" is user input. This allows for flexibility of breakpoint distance for various weapon systems on the battlefield.

E. THE PARAMETRIC TERRAIN

The terrain affects a great deal on detection, mobility, tactics, and intervisibility between weapon systems in ground combat environments. In the model, the battle is simulated on 3 x 4 Km piece of terrain represented as a part of the coastal area east of the Korean Peninsula. It is important to have a terrain representation to emulate actual terrain areas. The model uses the parametric terrain representation method which was proposed by Chris Needle [Ref. 8]. The idea of the parameterized terrain is that the elevation of any hill mass can be represented by a bivariate normal density function. Mathematically, if $f_I(X,Y)$ is a function giving the elevation of the I's hill masses at any X,Y map coordinates on the battlefield, the overall terrain elevation at X,Y is obtained as the positive maximum over all the hill masses,

$$Z = f(X,Y) = \text{maximum } f_I(X,Y) \\ I = 1, \dots, \text{NHILLS}$$

where NHILLS is the total number of hill masses on the battlefield. Then, elevation data is used to compute the existence of line of sight between opposing forces which is a key element in detection process. The model uses the line-of-sight routine which was written by Prof. James K. Hartmann [Ref. 5].

In order to represent a piece of real terrain with parametric terrain, it is necessary to fit hill mass functions $f_I(X,Y)$ to a contour map of the terrain to be modeled. The fitting

process can be done by comparing a computer generated contour map by varying the bivariate normal parameters to the original terrain map. The computer generated terrain map of the battle area is inclosed as Figure 6. Appendix D presents the program listing for plotting a contour map from hill mass functions. This program can be used for the user to fit a specific real terrain which he has in mind into the parameterized terrain.

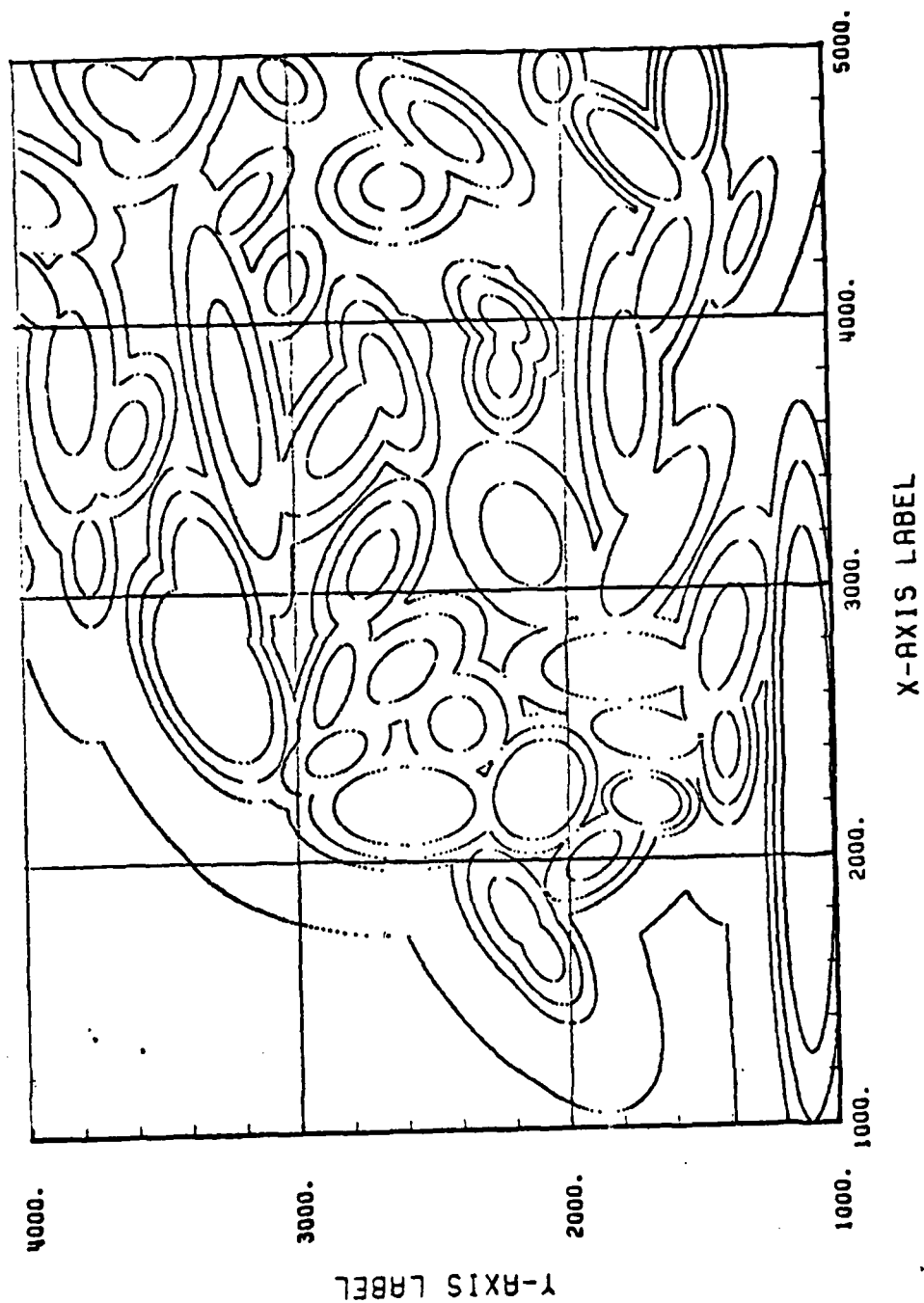


Figure 6. Model Terrain Map

IV. FINAL REMARKS

In order to illustrate basic modeling points for understanding and developing complex-operational amphibious-warfare models, a simplified model (specially tailored to a small-unit-amphibious-operation scenario) has been developed. Although several user options and varieties of modeling techniques have been incorporated into the model, the model should not be viewed as the final product.

There are several areas of model enhancement and enrichment that should be considered in the future. Only the aggregated amphibious task force fire support is played explicitly in the amphibious assault phase. The effect of artillery, naval gunfire and close air support during the various phases of amphibious operations should be added to the model. Ammunition consumption and resupply are considered vital to the success of any military operation, and such aspects should be also added to the model. Enemy forces should be played in greater detail. The movement of reacting enemy force and their dynamic-defensive-position selection are being considered for future model inclusion. A module which considers enemy reaction time, the terrain, and the tactical situation, and which dynamically determines which side is going to take the defensive role, as well as its defensive position, has been proposed to enhance the existing model. Inclusion of these features would create a more complicated model, adding realism but detracting from the current simple and transparent form.

The model currently simulates the ground combat on a 3 x 4 Km piece of coastal terrain representing an area of Ham-Hung, Korea. In order to simulate combat on a user's specific terrain, he needs to fit a parameterized terrain model to the actual terrain of interest. Doing so using the terrain fitting method described in the preceding chapter is an extremely tedious and time consuming process. The development of a more efficient terrain fitting technique will greatly enhance the model flexibility, and increase its utility in responding to interrogations from the real world.

The interested reader may obtain the model program deck and the sample input data deck from Prof. James G. Taylor, Naval Postgraduate School. Since the data used for the model run is hypothetical and greatly simplified, the reader is cautioned not to draw any analytical conclusions from the output.

APPENDIX A

SAMPLE EXPECTED OUTPUT

I. Amphibious Assault Summary

AMPHIBIOUS ASSAULT INFORMATION

INITIAL FORCE STRENGTH

WAVE	1	2	3	4	5
LVA	10.0	11.0	11.0	10.0	3.0

DT = 3.0 DS = 1.0

LVA ENGR SPECS

SPDMAX	SPDMIN	HTMAX	HTMIN	WID
10.30	3.50	1.70	0.60	3.53

DEFENSIVE TACTICAL PARAMETERS

	RANGE		AIM-RELOAD	PROJECTILE
	MAX	MIN	TIME	VELOCITY
TANK	1500.0		15.00	350.00
ATGM	2000.0	200.0	30.00	350.00

DEFENSIVE TACTICAL ALLOCATION WEIGHTS:

WAVE 1 = 2.00 WAVE 2 = 1.00

DEFENSIVE FORCE ATTRITION COEFFICIENTS

	ALPHA*A	BETA*A
DT	0.00006	0.00070
DS	0.00008	0.00090

WBETA(1) = 0.00050 WBETA(2) = 0.00070

BREAKPOINT ASSUMPTION: 0.3*(TOTAL DEP FORCE)

DEFENSIVE FORCE LEVEL FOR GROUND ATK 0.32

DISPERSION DATA

RANGE	TSIGV	RANGE	TSIGH	RANGE	TMEANH
25.0	0.0	25.0	0.0	25.0	0.0
500.0	2.0	500.0	2.0	500.0	1.0
1000.0	5.0	1000.0	5.0	1000.0	5.0
2000.0	20.0	2000.0	20.0	2000.0	10.0
5000.0	25.0	5000.0	25.0	5000.0	15.0
10000.0	25.0	10000.0	25.0	10000.0	15.0

RANGE	SSIGV	RANGE	SSIGH
25.0	0.0	25.0	0.0
250.0	5.0	250.0	5.0
500.0	7.5	500.0	7.5
1000.0	14.0	1000.0	14.0
2500.0	15.5	2500.0	15.5
5000.0	17.0	5000.0	17.0
10000.0	20.0	10000.0	20.0

II. Assault Phase Time Step Summary

TIME = 815.0 SECONDS

WAVE	FORCE LEVEL	STATUS	LOST-PCT	TSURV
1	0.7322	1	0.927	
2	1.7451	1	0.841	
3	4.5060	1	0.590	
4	9.8051	3	0.019	
5	3.0000	2	0.0	
TANK	0.0		1.000	19.79
ATGM	0.0		1.000	0.0
FINAL LVA SURVIVORS ASHORE =			19.788	
GROUND ATTACK STARTS AFTER DEFENDER BROKE CONTACT				
GROUND ATK TIME = 825.0				

III. Initial Ground Combat Summary

INITIAL GROUND COMBAT INFORMATION			
UNIT	X	Y	FORCE LEVEL
1	2000.0	1900.0	3.0
2	1900.0	2400.0	3.0
3	1500.0	2100.0	3.0
4	3800.0	2700.0	3.0
5	3800.0	2300.0	3.0
6	3600.0	1700.0	3.0

ATTRITION IS DETERMINISTIC

ROUTES DETERMINED BY USER

ATTACK VEHICLE SPEED IS 12.0

BREAKPOINT DISTANCE IS 500.0

DEFENDER WILL MOVE TO ALTERNATE POSITIONS
ALTERNATE POSITIONS ARE:

UNIT	X	Y
4	4500.0	3800.0
5	4500.0	2700.0
6	4600.0	1800.0

ATK KILL PROBABILITIES				
RANGE	P	PHH	PHM	PKH
500	0.85	0.85	0.75	0.70
1000	0.80	0.80	0.75	0.70
1500	0.75	0.75	0.70	0.65
2000	0.60	0.65	0.60	0.55
2500	0.45	0.50	0.50	0.35
3000	0.20	0.20	0.20	0.20

DEF. KILL PROBABILITIES				
RANGE	P	PHH	PHM	PKH
500	0.60	0.70	0.65	0.85
1000	0.85	0.90	0.85	0.90
1500	0.80	0.85	0.85	0.80
2000	0.75	0.80	0.75	0.70
2500	0.60	0.70	0.65	0.65
3000	0.40	0.45	0.40	0.50

IV. Ground Combat Time Step Summary

TIME = 1395 SECONDS

UNIT	X	Y	FORCE LEVEL	STATUS	LOST-PCT	TARGETS
1	2420.8	1984.2	0.0	2	1.000	
2	3664.1	2253.0	0.0	2	1.000	
3	4397.4	1742.2	2.9	0	0.038	
4	4500.0	3800.0	0.0	2	1.000	
5	4500.0	2700.0	2.8	0	0.055	
6	4600.0	1800.0	0.0	2	1.000	

* DISTANCE BETWEEN FORCES IS TOO CLOSE. END OF BATTLE

APPENDIX B

LISTING OF SAMPLE INPUTS

I. Amphibious Assault Input

1	1					
10.30	3.5	1.7	0.6	3.533		
10.						
1500.	2000.	200.				
15.	30.	350.	350.			
25.	500.	1000.	2000.	5000.	10000.	0.
2.	5.	20.	25.	25.		
25.	500.	1000.	2000.	5000.	10000.	0.
2.	5.	20.	25.	25.		
25.	500.	1000.	2000.	5000.	10000.	0.
1.	5.	10.	15.	15.		
25.	250.	500.	1000.	2500.	5000.	10000.
0.	5.	7.5	14.	15.5	17.	20.
25.	250.	500.	1000.	2500.	5000.	10000.
0.	5.	7.5	14.	15.5	17.	20.
2.	1.					
10.	11.	11.	10.	3.		
3.	1.					
0.00006	0.00008					
0.0007	0.0009					
0.0005	0.0007					
.32						
50.	100.					

II. Terrain Data

46					
0.					
2000.	1100.	170.	0.1	999.9	8.0
1800.	2200.	150.	30.	350.	2.0
2000.	1900.	150.	130.	300.	2.
2400.	1400.	150.	0.1	300.	2.5
2450.	1700.	130.	80.	500.	2.2
2700.	1800.	138.	90.	500.	2.2
3200.	1650.	140.	150.	600.	3.
4300.	1300.	130.	160.	400.	3.5
3750.	1750.	150.	0.1	660.	3.6
4150.	1600.	150.	160.	550.	3.
3200.	2150.	130.	25.	500.	1.5
4600.	1700.	170.	45.	300.	2.5
4800.	1500.	170.	0.1	300.	2.5
2200.	2600.	170.	90.	350.	1.8
2400.	2850.	150.	120.	300.	1.8
3100.	2700.	150.	150.	350.	2.

2500.	2400.	150.	0.1	250.	1.0
2650.	2850.	150.	160.	400.	3.0
2700.	2600.	150.	130.	370.	1.8
3800.	2200.	150.	0.1	230.	1.5
4500.	2600.	150.	90.	280.	1.3
3600.	2800.	150.	145.	500.	2.5
2700.	3300.	190.	25.	350.	2.0
3000.	3300.	170.	15.	400.	2.5
3150.	3750.	130.	0.1	350.	2.5
3750.	3200.	150.	10.	850.	5.0
3800.	3800.	150.	0.1	650.	3.
3600.	3600.	150.	160.	320.	3.0
4150.	3950.	170.	30.	220.	2.2
1650.	2100.	150.	30.	300.	2.0
2250.	2100.	180.	150.	220.	1.2
4000.	2200.	150.	45.	280.	2.
3900.	2200.	150.	0.1	300.	3.5
0	0	0	0	1	7
0	33	39	53	62	0
0	0	0	0	0	6
0	6	14	9	12	0
101					
1	2	3	30	4	43
6	32	33	7	11	31
8	9	10	11	33	43
8	42	2	14	30	23
16	17	18	19	20	3
2	31	11	16	20	22
46	20	21	22	12	34
42	45	46	14	23	15
26	14	25	26	27	28
35	44	26	27	29	35
40					

III. Ground Combat Input

```

1 28943
03 03
0000.0 2500.0 0500. 4000.0
3.0 3.0 3.0
1 2
2000.0 1900.0
1900.0 2400.0
1500.0 2100.0
01
5000.0 2500.0
01
4900.0 2150.0
02
2200.0 1700.0
4800.0 1750.0
3800.0 2700.0 3.0 190 120

```

3800.0 2300.0 3.0 190 120
3600.0 1700.0 3.0 180 120
0 0500.0 4
4500.0 3800.0
4500.0 2700.0
4600.0 1800.0
0.85 0.85 0.75 0.70
0.80 0.75 0.70 0.65
0.75 0.75 0.70 0.65
0.60 0.65 0.60 0.55
0.45 0.50 0.50 0.35
0.20 0.20 0.20 0.20
0.60 0.70 0.65 0.85
0.85 0.90 0.84 0.90
0.80 0.85 0.85 0.80
0.75 0.80 0.75 0.70
0.60 0.70 0.65 0.65
0.40 0.45 0.40 0.50

APPENDIX C

DEFINITION OF VARIABLES IN COMPUTER PROGRAM

1. The Amphibious Assault Phase

CDSURV(I) = Current strength of defensive force I
I = 1 TANK
I = 2 ATGM

CSURV(I) = Current strength of assault wave I

DA(I) = Attrition rate for def. unit I due to the effects of ATFFS/TLF

DS1 = That portion of the DS unit assigned to engaging the closer of two multiple waves in the ATGM engagement window

DS2 = That portion of the Ds unit assigned to engaging the farther of two multiple waves in the ATGM engagement window

DT1 = That portion of the Dt unit assigned to engaging the closer of two multiple waves in the TANK engagement window

DT2 = That portion of the DT unit assigned to engaging the farther of two multiple waves in the TANK engagement window

DT1PH = Hit probability of rounds fired by DT1 against wave TENG(1)

DT1ROF = Rate of fire utilized by DT1 against wave TENG(1)

DINIT = Initial strength of def. force I

IL(I) = When equal to 1 indicates the wave landed shore

IWPN = Weapon code: TANK = 1, ATGM = 2

IWSTAT(I) = Current status of wave I
0 - not engaging
1 - landed
2 - under fire by ATGM
3 - under fire by TANK
4 - under fire both ATGM and TANK

GALF = Denote whether the LF build-up is sufficient
 for the ground attack
 0 - not sufficient
 1 - sufficient

GATK = Denote whether the LF initiated the ground attack
 0 - not started yet
 1 - started already

GATM = Time when the ground attack started

RD = Distance offshore at which waves initiate
 transition

RKSURV(I) = Concatenation of CSURV and CDSURV

SA(I) = Attrition rate for wave I due to ATGM

SENG(I) = The wave number of the closer of two waves in
 the ATGM engagement window

SRNG(I) = Firing range to wave SENG(I)

SSIGH = The std dev error in the horizontal for ATGM

SSIGV = The std dev error in the vertical for ATGM

SWTS(I) = The proportion of the total DS strength to be
 allowed to engaging SENG(I)

TA(I) = Attrition rate for wave I due to TANK

TBW = The interarrival time between waves arriving at
 the beach

TMEANH = The bias error in the horizontal for TANK

TMEANV = The bias error in the vertical for TANK

TENG(I) = The wave number of the closer of two waves in
 the tank engagement window

TRNG(I) = the firing range to wave TENG(I)

TSIGH = The std dev error in the horizontal for TANK

TSIGV = The std dev error in the vertical for TANK

TSURV = Total number of surviving LVA at the current time

TWTS(I) = The proportion of the total DT strength to be
 allowed to engaging TENG(I)

WVINT(I) = Initial strength of wave I

2. The Ground Attack Phase

ALPHA(I) = Initial attrition-rate coefficient for stochastic attrition module

APOA(I,J) = The average proportion of the j^{th} attacker of unit i allocated to fire on unit i

AVSP = Average speed of moving attacking units

BREAK = Breakpoint distance between attacking units and defenders

DISMAX = Maximum distance allowed between attacking units before the leading unit is delayed

DIST = The straight-line distance between two movement nodes inputed by the user

DST = The distance in meters to be moved each time step by attacking units

FL(I) = Force level of unit i

FO(I) = Force level of unit i

FO(I) = Initial force level of unit i

IALT = Denotes whether the user desires alternate defensive positions or not
0 - yes
1 - no

IC = Counts number of time units a defender has been moving

IDIR(I,J) = Direction of j^{th} interval in i^{th} route

II(I) = Interval index for unit i

IMOVE = Number of time units a defender is allowed for moving to an alternate position

IPRDIR(I) = Primary direction of movement for unit i

IRTE = Denotes whether user wants to input routes or not
0 - program determined routes
1 - user determined routes

IS = Random number seed used for stochastic attrition

ISECWD(I) = Width of search sector for unit i

ISPD = Input variable to denote user's desired speed
for attackers movement
1 - 9 mph
2 - 12 mph
3 - 15 mph
4 - 18 mph

ITEM = Input variable denoting number of time steps
allowed for defender's move

ITIME = Current time, in seconds, of battle

ITRIT = Input variable denoting whether attrition
will be stochastic or deterministic
0 - stochastic
1 - deterministic

IUSTAT(I) = Current status of unit i
0 - unit alive, not firing
1 - unit alive and firing
2 - unit killed
3 - unit moving

LOA(I,J) = The number of the j^{th} attacker of unit i

LOST(I,J) = Denotes whether line-of-sight exists between
unit i and j or not

LOT(I,J) = The number of the j^{th} target of unit i

MVTDIR(I) = Movement direction of unit i

N(I) = Number of nodes inputed by user for route i

NA(I) = Number of attackers of unit i

NBU = Number of defense units

NF(I) = Number of time units i is allowed to fire at
the same location

NLOSC(I,J) = Number of continuous time steps that line-of-sight
does not exist between unit i and unit j

NOI(I) = Number of intervals in the i^{th} route

NRU = Number of attack units

NT(I) = Number of targets of unit i

OFL(I) = Force level of unit i during previous time step

$P(I,J)$ = Probability of 1st round hit by unit i in range band j
 $PHH(I,J)$ = Probability of a hit following a hit by unit i in range band j
 $PHM(I,J)$ = Probability of a hit following a miss by unit i in range band j
 $PKH(I,J)$ = Probability of a kill given a hit by unit i in range band j
 PM = The proportion of time a moving unit is searching for targets
 $POA(I,J)$ = The proportion of the jth attacker of unit i allocated to fire on unit i
 $POL(I)$ = Percent of unit i lost during the current time step
 $PTT(I)$ = Proportion of surviving firepower allocated to the ith target if there are j targets available
 $RANGE$ = Current minimum distance between attackers and defenders
 $Q(I,J)$ = Probability that unit j is not detected by unit i at current time
 RF = Detection rate reduction factor for a firing unit (in comparison with non-firing unit)
 $RMINTK$ = Minimum effective range for defending weapon system
 $RMINTW$ = Minimum effective range for attacking weapon system
 $RMXTK$ = Maximum effective range for defending weapon system
 $RMXTW$ = Maximum effective range for attacking weapon system
 $ROT(I,J)$ = The range of the jth target of unit i
 $SIZETK$ = Size of attacking vehicle
 $SIZETW$ = Size of defending vehicle
 $TA(K)$ = Time to acquire a target for kth weapon system type (k = 1,2)
 $TF1(K)$ = Time of flight to 1000m for kth weapon system type (k = 1,2)

TF2(K) = Time of flight to 2000m for k^{th} weapon system type ($k = 1,2$)
 TF3(K) = Time of flight to 3000m for k^{th} weapon system type ($k = 1,2$)
 TH(K) = Time to fire a round following a hit for weapon system type k ($k = 1,2$)
 TI(K) = Time to fire first round after target has been acquired for weapon system type k ($k = 1,2$)
 TM(K) = Time to fire a round following a miss for weapon system type k ($k = 1,2$)
 TNKFR = Firing rate for attacking weapon system
 TOWFR = Firing rate for defending weapon system
 TPOL(I) = Total percentage of lost since battle began for unit i
 VISFR(I,J) = The fraction of unit i seen by unit j
 VISFRA = Fraction of unit A as seen by unit B
 VISFRB = Fraction of unit B as seen by unit A
 X(I),Y(I) = Coordinates of unit i
 XA(I),YA(I) = Coordinates of alternate position for defender i
 XIC(I,J) = Coordinates of the j^{th} interval endpoint of the route for unit i
 YIC(I,J)
 XL,YL = Distance added to previous interval endpoint for vehicle to move DST during a time step
 XLOC(I,J) = Coordinates of the j^{th} node inputed by the user for the route of unit i
 YLOC(I,J)

PROGRAM LISTING

56

GRA00420
 GRA00430
 GRA00440
 GRA00450
 GRA00460
 GRA00470
 GRA00480
 GRA00490
 GRA00500
 GRA00510
 GRA00520
 GRA00530
 GRA00540
 GRA00550
 GRA00560
 GRA00570
 GRA00580
 GRA00590
 GRA00600
 GRA00610
 GRA00620
 GRA00630
 GRA00640
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 GRA00660
 GRA00670
 GRA00680
 GRA00690
 GRA00700
 GRA00710
 GRA00720
 GRA00730
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 GRA00770
 GRA00780
 GRA00790
 GRA00800
 GRA00810
 GRA00820
 GRA00830
 GRA00840
 GRA00850
 GRA00860
 GRA00870
 GRA00880
 GRA00890

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106 IF(GATK-2.0) 10,20,30
107 WRITE(6,107)
108 FORMAT(IX,'GROUND ATTACK STARTS WHILE SHORE COMBAT IS GOING ON')
109 GO TO 110
20 WRITE(6,108)
108 FORMAT(IX,'GROUND ATTACK STARTS AFTER DEFENDER BROKE CONTACT')
109 GO TO 110
30 WRITE(6,109)
109 FORMAT(IX,'GROUND ATTACK STARTS AFTER ALL WAVES LANDED')
110 WRITE(6,111) GATM
111 FCRMAT(/IX,'GROUND ATK TIME=',F6.1)
    CALL GROUND(GATM)
    STOP
    END

C
SUBROUTINE SEA(GATM,GATK)
COMMON /AMPH/IL(5),WB(2),A(2),B(2),ITE,ISE,RD,WVINT(5),WID,
1TBW,DINT(2),GAINL,IWSTAT(5)
COMMON /ENGR/ SPDMAX,SPDMIN,HTMIN,TTS,IAA,TB,TFF
CALL OUTPUT
IRD=500
ITBW=120
RD=1.0*IRD
TBW=1.0*ITBW
TINT=0.0

C
COMPUTATION OF FIRST WAVE TIME PARAMETERS
TA-TIME FIRST WAVE INITIATES TRANSITION
TB-TIME FIRST WAVE COMPLETES TRANSITION
TFF-TIME FIRST WAVE REACHES THE BEACH

TAA=(5000.-RD)/SPDMAX
TB=TAA+TTS
TFF=TB+(RD-(0.5*(SPDMAX-SPDMIN)*TTS)-150.)/SPDMIN
DEL=10.
WRITE(6,55) RD,TBW
55 FORMAT(/,IX,'ITERATION INITIATED...RD=',F10.3,IX,'TBW=
1. F10.3)
CALL RKINT(DEL,TINT,N,GATM,GATK)
RETURN
END
SUBROUTINE RKINT(H,TI,N,GATM,GATK)

C
SUBROUTINE RKINT PROVIDES THE INTERFACE BETWEEN
THE EULER NUMERICAL INTEGRATION ROUTINE(RKLEQ)
AND THE SUBROUTINE ATTR WHICH DETERMINES EACH
UNIT'S STATUS AS TIME PROGRESSES THROUGH THE
  
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      RKSURV(I+5)=CDSURV(I)
45  RKATTR(I+5)=-1.0*DA(I)
      S=RKLDQ(7,RKSURV,RKATTR,T,H,NT)
      DC 50 I=1,5
      CSURV(I)=RKSURV(I)
50  CONTINUE
      DO 55 I=1,2
      CDSURV(I)=RKSURV(I+5)
55  CONTINUE
      IF(S-1.) 1100,1000,1200
1100 WRITE(6,60)
60  FCRMAT(IX,ERRO..S.NE.1.OR.2)
      STOP
1200 CONTINUE
      IT=IT+1
      TSURV=0.
      DO 65 L=1,5
      TSURV=TSURV+CSURV(L)
65  IF(TSURV.LE.0.) TSURV=0.
      TIME(IT)=T
      C PRINT RESULT OF SHIP TO SHORE MOVEMENT AFTER EACH TIME STEP
112 WRITE(6,112) T,TIME=F6.1,1X,'SECONDS'///)
113 WRITE(6,113)
113 FORMAT(IX,'WAVE',2X,'FORCE LEVEL',2X,'STATUS',2X,'LOST-PCT',
12X,TSURV)
      DO 66 I=1,4
      PLOST=1.-CSURV(I)/WVINT(I)
114 WRITE(6,114) I,CSURV(I),IWSTAT(I),PLOST
66  FORMAT(3X,11,3X,F10.4,5X,11,5X,F8.3)
      CONTINUE
      PLOST=1.-CSURV(5)/WVINT(5)
115 WRITE(6,115) CSURV(5),IWSTAT(5),PLOST,TSURV
      FORMAT(3X,5,3X,F10.4,5X,11,5X,F8.3,2X,F5.2)
      PLOST=1.-CDSURV(1)/DINIT(1)
116 WRITE(6,116) CDSURV(1),PLOST
      FORMAT(IX,'TANK',2X,F10.4,11X,F8.3)
      PLOST=1.-CDSURV(2)/DINIT(2)
      TSURV=CDSURV(1)+CDSURV(2)
117 WRITE(6,117) CDSURV(2),PLOST,TASURV
      FORMAT(IX,'ATGM',2X,F10.4,11X,F8.3,2X,F5.2)
      C
      DO 80 J=1,5
      TATTR(IT,J)=TA(J)
80  TATTR(IT,J+5)=SA(J)
      DO 85 J=1,2
85  TATTR(IT,J+10)=DA(J)
      R=RNG(I-4,*IBW)

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GRA01380
GRA01390
GRA01400
GRA01410
GRA01420
GRA01430
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GRA01450
GRA01460
GRA01470
GRA01480
GRA01490
GRA01500
GRA01510
GRA01520
GRA01530
GRA01540
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GRA01570
GRA01580
GRA01590
GRA01600
GRA01610
GRA01620
GRA01630
GRA01640
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GRA01670
GRA01680
GRA01690
GRA01700
GRA01710
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GRA01850

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GRA01860
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GRA01970
GRA01980
GRA01990
GRA02000
GRA02010
GRA02020
GRA02030
GRA02040
GRA02050
GRA02060
GRA02070
GRA02080
GRA02090
GRA02100
GRA02110
GRA02120
GRA02130
GRA02140
GRA02150
GRA02160
GRA02170
GRA02180
GRA02190
GRA02200
GRA02210
GRA02220
GRA02230
GRA02240
GRA02250
GRA02260
GRA02270
GRA02280
GRA02290
GRA02300
GRA02310
GRA02320
GRA02330

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C  DETERMINE IF ALL WAVES LANDED AND GROUND ATK STARTED
C  IF(R.LT.75.) GO TO 2000
    IF(I1.GT.IMAX) GO TO 2000
    IF(I1.EQ.99) GO TO 2000
    GO TO 1000
2000 N=I1
    WRITE(6,90) TSURV
    FORMAT(IX,F10.3)
    IF(GATK.GE.1.) GO TO 2222
    IF(TSURV.LT.9.) GO TO 2222
    GATK=3.
    GATM=T
    RETURN
2222 END
    FUNCTION RKLDEQ(N,Y,F,X,H,NT)
    DIMENSION Y(1),F(1),Q(25)
    NT=NT+1
    GO TO (1,2,3,4),NT
    1  H1=H
       AA=H1/4.0
       DO 11 J=1,N
          11 Q(J)=0.
          X=X+AA
          GO TO 5
          2  X=X+AA
          GO TO 5
          3  X=X+AA
          GO TO 5
          4  DO 93 L=1,N
             93 Y(L)=Y(L)+AA*F(L)
             NT=0
             X=X+AA
             RKLDEQ=2.
             GO TO 6
          5  DO 90 I=1,N
             90 Y(I)=Y(I)+AA*F(I)
             6  RETURN
          6  END
    SUBROUTINE ATTR(T,CSURV,DSURV,TA,SA,DA,GALF,GATK,GATM)
C  GIVEN THE CURRENT TIME AND STATE VARIABLE STRENGTHS,
C  SUBROUTINE ATTR DETERMINES THE ATTRITION RATES AND UPDATES
C  THE STATUS OF EACH UNIT WITH RESPECT TO SHORE MOVEMENT
C  AND IMPLEMENTS THIS INFORMATION INTO THE ATTRITION LOSS RATE
C  COMPUTATION.

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C TA(1) - CURRENT ATTRITION LOSS RATE FOR WAVE 1 DUE TO TANK FIRE
C SA(1) - CURRENT ATTRITION LOSS RATE FOR WAVE 1 DUE TO ATGM FIRE
C DA(1) - CURRENT ATTRITION LOSS RATE FOR DEF. FORCE 1 DUE TO
C ATFFS(AMPHIBIOUS TASK FORCE FIRE SUPPORT)/TLF EFFECTS
C
C COMMON /AMPH/IL(5),WB(2),A(2),B(2),ITE,ISE,RD,WVINT(5),WID,
C 1TBW,DINIT(2),GAINL,IWSTAT(5)
C COMMON /DEF/TENGMX,SENGMX,TARTM,SARTM,TVEL,
C 1SVEL,DEFWTS(2)
C 1INTEGER TENG(2),SENG(2)
C 1DIMENSION TRNG(2),TWTS(2),SRNG(2),DSURV(2),SWTS(2),
C 1CSURV(5),TA(5),SA(5),DA(2)
C
C DO 10 I=1,5
C TA(I)=0.
C SA(I)=0.
C 10 CONTINUE
C
C DS1=0.
C DS2=0.
C DT1=0.
C DT2=0.
C FAC=1.0
C
C DETERMINE IF PART OF LANDING FORCE ADVANCE TO ATTACK INLAND
C KEY TERRAIN
C
C IF(GATK.EQ.1.0) GO TO 2929
C IF(GALF.EQ.1.0.AND.(DSURV(1)+DSURV(2)).LE.GAINL*(DINIT(1)
C 1+DINIT(2))) GATM=T
C IF(GALF.EQ.1.0.AND.(DSURV(1)+DSURV(2)).LE.GAINL*(DINIT(1)
C 1+DINIT(2))) GATK=1.0
C
C DETERMINE IF DEF. BREAKPOINT HAS BEEN REACHED
C
C 2929 IF((DSURV(1)+DSURV(2)).LT.0.3*(DINIT(1)+DINIT(2)))
C 1 GO TO 20
C
C DETERMINE ATTRITION RATE ON DEFENSIVE FORCES BY ATFFS
C BASED UPON AREA OR AIMED FIRE STATUS
C
C DA(1)=B(1)
C DA(2)=B(2)
C IF(ITE.EQ.0) DA(1)=A(1)+DSURV(1)
C IF(ISE.EQ.0) DA(2)=A(2)+DSURV(2)
C GO TO 30

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GRA02340
 GRA02350
 GRA02360
 GRA02370
 GRA02380
 GRA02390
 GRA02400
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 GRA02420
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 GRA02970
 GRA02980
 GRA02990
 GRA03000
 GRA03010
 GRA03020
 GRA03030
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 GRA03070
 GRA03080
 GRA03090
 GRA03100
 GRA03110
 GRA03120
 GRA03130
 GRA03140
 GRA03150
 GRA03160
 GRA03170
 GRA03180
 GRA03190
 GRA03200
 GRA03210
 GRA03220
 GRA03230
 GRA03240
 GRA03250
 GRA03260
 GRA03270
 GRA03280
 GRA03290

```

20 DSURV(1)=0.
   DSURV(2)=0.
   DA(1)=0.
   DA(2)=0.
   IF(GATK.EQ.1.) GO TO 3939
   GAT=T

C   DETERMINE IF DEF-BREAKPOINT HAS BEEN REACHED BEFORE SUFFICIENT
C   LANDING FORCE IS BUILT UP ON THE SHORE FOR INLAND ATTACK
C

97 DO 91 I=1,5
   WVRNG=RNG(GAT-TBW*(I-1))
   IF(WVRNG.LT.75.) IL(I)=1
   IF(IL(I).EQ.1.) TLF=TLF+CSURV(I)

91 CONTINUE
   GAT=GAT+10.
   IF(TLF.LT.9.0.AND.IL(5).EQ.1) RETURN
   IF(TLF.LT.9.0.AND.IL(5).NE.1) GO TO 97
   GATK=2.
   GATF=1.
   GATM=GAT
   WRITE(6,220) GATM
220 FORMAT(/,1X,'GROUND ATK INITIATES AT TIME=',F7.1)
3939 IL(1)=99
25 WRITE(6,25) T
   FORMAT(1X,'BEAKPOINT REACHED AT TIME = ',F9.3)
   RETURN
30 CALL DTGTS(T,TENG,TRNG,TWTS,SENG,SRNG,SWTS,CSURV)

C   DETERMINE THE CUMULATIVE NUMBER OF SURVIVING LVA'S
C   THAT HAVE BEEN REACHED THE BEACH - TLF
C
   TLF=0.
   DO 40 J=1,5
     IF(IL(J).EQ.1) TLF=TLF+CSURV(J)
40 CONTINUE

C   DETERMINE IF TLF BUILT UP IS SUFFICIENT FOR GROUND ATK
C
   IF(TLF.GE.9.) GATF=1.
   IF(GATK.EQ.1.) TLF=TLF-9.

C   ALLOCATE THE FORCE STRENGTH OF TLF BETWEEN THE TWO
C   DEFENSIVE FORCE UNITS
C
   DSUM=DSURV(1)+DSURV(2)
   TLF1=(DSURV(1)/DSUM)*TLF
   TLF2=(DSURV(2)/DSUM)*TLF
  
```

GRA03300
 GRA03310
 GRA03320
 GRA03330
 GRA03340
 GRA03350
 GRA03360
 GRA03370
 GRA03380
 GRA03390
 GRA03400
 GRA03410
 GRA03420
 GRA03430
 GRA03440
 GRA03450
 GRA03460
 GRA03470
 GRA03480
 GRA03490
 GRA03500
 GRA03510
 GRA03520
 GRA03530
 GRA03540
 GRA03550
 GRA03560
 GRA03570
 GRA03580
 GRA03590
 GRA03600
 GRA03610
 GRA03620
 GRA03630
 GRA03640
 GRA03650
 GRA03660
 GRA03670
 GRA03680
 GRA03690
 GRA03700
 GRA03710
 GRA03720
 GRA03730
 GRA03740
 GRA03750
 GRA03760
 GRA03770

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C      ADD TO DA1 AND DA2 THE ATTRITION LOSS RATE DUE
C      TO THE EFFECTS OF TLF1 AND TLF2
C
C      DA{1}=DA{1}+TLF1*WB{1}
C      DA{2}=DA{2}+TLF2*WB{2}
C      IF{DSURV{1}.LE.0.0} DA{1}=0.0
C      IF{DSURV{2}.LE.0.0} DA{2}=0.0
C
C      DETERMINE IF THERE EXISTS AN INCOMING WAVE IN THE
C      TANK ENGAGEMENT WINDOW I.E. TENG(1).NE.0
C      IF(TENG(1).EQ.0.) GO TO 100
C      ITE=1
C
C      DETERMINE THE TIME SINCE WAVE TENG(1) CROSSED THE
C      5000. METER OFFSHORE MARK -T1
C      T1=T-TBW*(TENG(1)-1)
C      DT1=TWTS(1)*DSURV(1)
C      FAC=1.
C
C      DETERMINE THE SUPPRESSION EFFECT TO BE IMPOSED
C      ON THE DT UNIT BASED ON THE ATTRITION LOSS RATE
C      CURRENTLY IN EFFECT
C      SUPFAC=DA(1)
C
C      CALL RATE(TRNG(1),SPD(T1),1,SUPFAC,DT1ROF)
C      CALL PHIT(TRNG(1),WID,HT(T1),1,SUPFAC,DT1PH)
C
C      DETERMINE THE ATTRITION LOSS RATE FOR WAVE TENG(1)
C      DUE TO DT1 FIRES
C      TA(TENG(1))=DT1PH*DT1ROF*DT1
C
C      DETERMINE IF THERE IS A SECOND INCOMING WAVE THAT
C      IS IN THE TANK ENGAGEMENT WINDOW, IF THERE IS THE
C      ATTRITION RATE COMPUTATIONS ARE SIMILAR IN FORM
C      TC THOSE PREVIOUSLY PERFORMED FOR THE CLOSER WAVE
C      IF(TENG(2).EQ.0) GO TO 100
C      T2=T-TBW*(TENG(2)-1)
C      DT2=TWTS(2)*DSURV(1)
C      CALL RATE(TRNG(2),SPD(T2),1,SUPFAC,DT2ROF)
C      CALL PHIT(TRNG(2),WID,HT(T2),1,SUPFAC,DT2PH)
C      TA(TENG(2))=DT2PH*DT2ROF*DT2
C
  
```


GRA04260
 GRA04270
 GRA04280
 GRA04290
 GRA04300
 GRA04310
 GRA04320
 GRA04330
 GRA04340
 GRA04350
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 GRA04370
 GRA04380
 GRA04390
 GRA04400
 GRA04410
 GRA04420
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 GRA04500
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 GRA04570
 GRA04580
 GRA04590
 GRA04600
 GRA04610
 GRA04620
 GRA04630
 GRA04640
 GRA04650
 GRA04660
 GRA04670
 GRA04680
 GRA04690
 GRA04700
 GRA04710
 GRA04720
 GRA04730

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DO 100 I=1,5
WVRNG=RNG(I-TBW*(I-1))
IF(WVRNG.LT.75.) IL(I)=1
IF(WVRNG.LT.75.) IWSTAT(I)=1

IF THE FIRING RANGE TO A WAVE IS LESS THAN 75 METERS,
THE WAVE IS CONSIDERED TO HAVE REACHED A COVERED AND
CONCEALED POSITION ON THE BEACH

IF((WVRNG.GT.TENGMX).OR.(CSURV(I).LT.0.05).OR.
1(WVRNG.LT.75.).OR.(JT.GE.2)) GO TO 50
JT=JT+1
TENG(JT)=1
TWTS(JT)=DEFWTS(JT)*CSURV(I)
TSUM=TSUM+TWTS(JT)
TRNG(JT)=WVRNG
50 IF((WVRNG.GT.SENGMX).OR.(CSURV(I).LT.0.05).CR.
1(WVRNG.LT.SENGMN).OR.(JS.GE.2)) GO TO 100
JS=JS+1
SENG(JS)=1
SRNG(JS)=WVRNG
SWTS(JS)=DEFWTS(JS)*CSURV(I)
SSUM=SSUM+SWTS(JS)
100 CONTINUE

C DETERMINE WAVE STATUS
C
DO 20 I=1,2
DO 25 J=1,5
IF(IWSTAT(I,J).NE.1.AND.SENG(I).EQ.J) IWSTAT(J)=2
25 CONTINUE
20 CONTINUE
DO 30 I=1,2
DO 35 J=1,5
IF(IWSTAT(I,J).EQ.1) GO TO 35
IF(IWSTAT(I,J).EQ.2.AND.TENG(I).EQ.J) IWSTAT(J)=4
IF(IWSTAT(I,J).NE.2.AND.TENG(I).EQ.J) IWSTAT(J)=3
35 CONTINUE
30 CONTINUE

C
IF(TENG(I).EQ.0) GO TO 500
DO 200 I=1,2
TWTS(I)=TWTS(I)/TSUM
200 CONTINUE
500 IF(SENG(I).EQ.0) RETURN
DO 600 I=1,2
SWTS(I)=SWTS(I)/SSUM
600 CONTINUE
  
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GRA04740
 GRA04750
 GRA04760
 GRA04770
 GRA04780
 GRA04790
 GRA04800
 GRA04810
 GRA04820
 GRA04830
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 GRA04850
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 GRA04910
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 GRA04980
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 GRA05000
 GRA05010
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 GRA05090
 GRA05100
 GRA05110
 GRA05120
 GRA05130
 GRA05140
 GRA05150
 GRA05160
 GRA05170
 GRA05180
 GRA05190
 GRA05200
 GRA05210

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C
RETURN
END
SUBROUTINE DATAIN
COMMON /AMPH/IL(5),WB(2),A(2),B(2),ITE,ISE,RD,WVINT(5),WID,
1TBW,DINIT(2),GAINL,IWSTAT(5)
COMMON /ENGR/SPDMAX,SPDMIN,HTMAX,HTMIN,TTS,TAA,TB,TFF
COMMON /DISPER/TSIGV(6,2),TSIGH(6,2),TMEANH(6,2),
1SSIGV(7,2),SSIGH(7,2)
COMMON /DEF/TENGMX,SENGMX,TARTM,SARTM,TVEL,
1SVEL,DEFWTS(2)
COMMON /SUPEFT/GAMMA,DELTA
COMMON /IOUT/ISURV,IATTR
READ(5,50) ISURV,IATTR
READ(5,100) SPDMAX,SPDMIN,HTMAX,HTMIN,WID
READ(5,100) TTS
READ(5,100) TENGMX,SENGMX
READ(5,100) TARTM,SARTM,TVEL,SVEL
READ(5,100) ((TSIGV(I,J),I=1,6),J=1,2)
READ(5,100) ((TSIGH(I,J),I=1,6),J=1,2)
READ(5,100) ((TMEANH(I,J),I=1,6),J=1,2)
READ(5,100) ((SSIGV(I,J),I=1,7),J=1,2)
READ(5,100) ((SSIGH(I,J),I=1,7),J=1,2)
READ(5,100) (DEFWTS(I),I=1,2)
READ(5,103) (WVINT(I),I=1,5)
READ(5,100) (DINIT(I),I=1,2)
READ(5,101) (A(I),I=1,2)
READ(5,101) (B(I),I=1,2)
READ(5,101) (WB(I),I=1,2)
READ(5,110) GAINL
READ(5,101) GAMMA,DELTA
FORMAT(F5.2)
110 FORMAT(2I5)
150 FORMAT(7F10.3)
101 FORMAT(2F10.5)
103 FORMAT(5F10.5)
RETURN
END

C
SUBROUTINE OUTPUT
COMMON /AMPH/IL(5),WB(2),A(2),B(2),ITE,ISE,RD,WVINT(5),WID,
1TBW,DINIT(2),GAINL,IWSTAT(5)
COMMON /DISPER/TSIGV(6,2),TSIGH(6,2),TMEANH(6,2),
1SSIGV(7,2),SSIGH(7,2)
COMMON /ENGR/SPDMAX,SPDMIN,HTMAX,HTMIN,TTS,TAA,TB,TFF
COMMON /DEF/TENGMX,SENGMX,TARTM,SARTM,TVEL,
1SVEL,DEFWTS(2)
COMMON /SUPEFT/GAMMA,DELTA
  
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C*** INPUT SUMMARY PRINTOUT
C
20 WRITE(6,20)
  FORMAT(1,1,1X,'AMPHIBIOUS ASSAULT INFORMATION')
22 WRITE(6,22)
  FORMAT(1,1X,'INITIAL FORCE STRENGTH')
23 WRITE(6,23)
  FORMAT(1,1,1X,'WAVE',2X,1,1,5X,'2',5X,'3',5X,'4',5X,'5')
24 WRITE(6,24)
  FORMAT(1,1,1X,'LVA',5(2X,F4.1))
21 WRITE(6,21)
  FORMAT(1,1,1X,'DT',1,1,5X,'DS',1,1X,F3.1)
25 WRITE(6,25)
  FORMAT(1,1X,'LVA ENGR SPECS')
26 WRITE(6,26)
  FORMAT(1,1,1X,'SPD MAX',2X,'SPD MIN',3X,'HT MAX',2X,'HT MIN',3X,'WID')
27 WRITE(6,27)
  FORMAT(2,1,1X,'SPD MAX',2X,'SPD MIN',2X,'HT MAX',2X,'HT MIN',2X,'WID')
630 WRITE(6,630)
  FORMAT(1,1X,'DEFENSIVE TACTICAL PARAMETERS')
631 WRITE(6,631)
  FORMAT(1,1X,'RANGE',4X,'AIM-RELOAD',3X,'PROJECTILE')
632 WRITE(6,632)
  FORMAT(1,1X,'MAX',3X,'MIN',4X,'TIME',7X,'VELOCITY')
633 WRITE(6,633)
  FORMAT(1,1X,'TANK',1X,F6.1,9X,F5.2,7X,F6.2)
634 WRITE(6,634)
  FORMAT(1,1X,'ATGM',1X,F6.1,1X,F6.1,2X,F5.2,7X,F6.2)
50 WRITE(6,50)
  FORMAT(1,1X,'DEFENSIVE TACTICAL ALLOCATION WEIGHTS:',1,1X,'WAVE 1',F5.2,1X,'WAVE 2',F5.2)
100 WRITE(6,100)
  FORMAT(1,1X,'DEFENSIVE FORCE ATTRITION COEFFICIENTS')
101 WRITE(6,101)
  FORMAT(1,1X,'ALPHA',10X,'BETA',10X)
102 WRITE(6,102)
  FORMAT(1,1X,'DT',6X,F7.5,9X,F7.5)
103 WRITE(6,103)
  FORMAT(1,1X,'DS',6X,F7.5,9X,F7.5)
104 WRITE(6,104)
  FORMAT(1,1X,'WB(1)',F7.5,1X,'WB(2)',F7.5)
105 WRITE(6,105)
  FORMAT(1,1X,'BREAKPOINT ASSUMPTION: 0.3*(TOTAL DEF FORCE)')
770 WRITE(6,770)
  FORMAT(1,1X,'DEFENDER ATTRITION LEVEL ALLOWING GROUND ATTACK',1,1X,F5.2,1X,'TOTAL DEFENDER FORCE')
  WRITE(6,771)
    GAMMA,DELTA

```

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GRA05220
GRA05230
GRA05240
GRA05250
GRA05260
GRA05270
GRA05280
GRA05290
GRA05300
GRA05310
GRA05320
GRA05330
GRA05340
GRA05350
GRA05360
GRA05370
GRA05380
GRA05390
GRA05400
GRA05410
GRA05420
GRA05430
GRA05440
GRA05450
GRA05460
GRA05470
GRA05480
GRA05490
GRA05500
GRA05510
GRA05520
GRA05530
GRA05540
GRA05550
GRA05560
GRA05570
GRA05580
GRA05590
GRA05600
GRA05610
GRA05620
GRA05630
GRA05640
GRA05650
GRA05660
GRA05670
GRA05680
GRA05690

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```

771 FORMAT(/IX,'ARTM SUP FACTOR=',F5.1,2X,'ERROR SUP FACTOR=',F5.1)
C**** DISPERSION DATA PRINTOUT
C
IDISP=1
IF (IDISP.EQ.0) RETURN
WRITE(6,601)
601 FORMAT(/IX,'DISPERSION DATA'/)
602 WRITE(6,602)
602 FORMAT(3X,'RANGE',2X,'TSIGV',2X,'RANGE',2X,'TSIGH',
12X,'RANGE',2X,'TMEANH')
DO 55 I=1,6
WRITE(6,603) TSIGV(I,1),TSIGV(I,2),TSIGH(I,1),TSIGH(I,2),
1TMEANH(I,1),TMEANH(I,2)
55 CONTINUE
603 FORMAT(1X,F7.1,2X,F5.1,1X,F7.1,1X,F5.1,1X,F7.1,1X,F5.1)
604 WRITE(6,604)
604 FORMAT(3X,'RANGE',2X,'SSIGV',2X,'RANGE',2X,'SSIGH')
DO 56 I=1,7
WRITE(6,605) SSIGV(I,1),SSIGV(I,2),SSIGH(I,1),SSIGH(I,2)
56 CONTINUE
605 FORMAT(1X,F7.1,2X,F5.1,1X,F7.1,1X,F5.1)
606 WRITE(6,606)
606 FORMAT(1,'THE AMPHIBIOUS ASSAULT PHASE BEGINS'////)
RETURN
END
C
SUBROUTINE PHIT(RANGE,W,H,IWPN,SUPFAC,PRHIT)
COMMON /AMPH/IL(5),WB(2),A(2),B(2),ITE,ISE,RD,WVINT(5),WID,
1TEW,DINIT(2),GAINL,IWSTAT(5)
COMMON /DISPER/TSIGV(6,2),TSIGH(6,2),TMEANH(6,2),
1SSIGV(7,2),SSIGH(7,2)
COMMON /SUPEFT/GAMMA,DELTA
C
PI=ACOS(-1.0)
IF(RANGE.LT.25.) STOP
IF(IWPN.EQ.1) GO TO 50
C ATGM FIRING DATA COMPUTATIONS
WMEANH=0.0
WMEANV=0.0
CALL INTRP(SSIGV,RANGE,WSIGV,7)
CALL INTRP(SSIGV,RANGE,WSIGV,7)
C TANK FIRING DATA COMPUTATIONS
WMEANH=0.0
WMEANV=0.0
CALL INTRP(TMEANH,RANGE,WMEANH,6)
CALL INTRP(TSIGV,RANGE,WSIGV,6)
CALL INTRP(TSIGH,RANGE,WSIGV,6)
C CONVERSION TO MILS

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GRA05700
GRA05710
GRA05720
GRA05730
GRA05740
GRA05750
GRA05760
GRA05770
GRA05780
GRA05790
GRA05800
GRA05810
GRA05820
GRA05830
GRA05840
GRA05850
GRA05860
GRA05870
GRA05880
GRA05890
GRA05900
GRA05910
GRA05920
GRA05930
GRA05940
GRA05950
GRA05960
GRA05970
GRA05980
GRA05990
GRA06000
GRA06010
GRA06020
GRA06030
GRA06040
GRA06050
GRA06060
GRA06070
GRA06080
GRA06090
GRA06100
GRA06110
GRA06120
GRA06130
GRA06140
GRA06150
GRA06160
GRA06170

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100 Z=AR SIN(H/RANGE)
WSIGV=WSIGV*(1.+DELTA*SUPFAC)
WSIGH=WSIGH*(1.+DELTA*SUPFAC)
TGTW={Z*6400.0)/(2.0*PI)
TGTW={AR SIN(W/RANGE)}*(6400.0/(2.0*PI))

C INSTITUTE NORMALITY ASSUMPTIONS TO CCMPUTE HORIZONTAL
C AND VERTICAL HIT PROBABILITIES
C
C=-1.0*SQRT(1./2.)
HOR1=((TGTW/2.)-WMEANH)/WSIGH
HOR2=((-1.0*TGTW)/2.0)-WMEANH/WSIGH
PHITX=1.0
IF (ABS(HOR1).GT.8.) GO TO 810
PHITX=0.5*(ERFC(C*HOR1))-ERFC(C*HOR2))
810 VER1=((TGTW/2.)-WMEANH)/WSIGV
VER2=((-1.0*TGTW)/2.)-WMEANH/WSIGV
PHITY=1.0
IF (ABS(VER1).GT.8.) GO TO 820
PHITY=0.5*(ERFC(C*VER1))-ERFC(C*VER2))
820 PRHIT=PHITX*PHITY
RETURN
END

C
C SUBROUTINE INTRP(X,ARG,VAL,N)
C DIMENSION X(N,2)
C WRITE(6,777) ARG
C 777 FORMAT(IX,ARG***)=,F10.3)
C IF (ARG.LT.X(1,1)) GO TO 500
C DO 50 I=1,N
C IF (ARG.GT.X(I+1,1)) GO TO 50
C DIFF=X(I+1,1)-X(I,1)
C DELTA=ARG-X(I,1)
C VAL=X(I,2)+(DELTA/DIFF)*(X(I+1,2)-X(I,2))
C RETURN
C 50 CONTINUE
C IF (ARG.GT.X(N,1)) GO TO 600
C VAL=X(N,2)
C RETURN
C 600 WRITE(6,601)
C 601 FORMAT(,ERROR IN INTRP ARG.GT.X(N,2),)
C STOP
C 500 WRITE(6,501)
C 501 FORMAT(,ERROR IN INTRP ARG.LT.X(1,1),)
C STOP
C END
C SUBROUTINE RATE(RANGE,SPEED,IWPN,SUPFAC,ROF)

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GRA06180
GRA06190
GRA06200
GRA06210
GRA06220
GRA06230
GRA06240
GRA06250
GRA06260
GRA06270
GRA06280
GRA06290
GRA06300
GRA06310
GRA06320
GRA06330
GRA06340
GRA06350
GRA06360
GRA06370
GRA06380
GRA06390
GRA06400
GRA06410
GRA06420
GRA06430
GRA06440
GRA06450
GRA06460
GRA06470
GRA06480
GRA06490
GRA06500
GRA06510
GRA06520
GRA06530
GRA06540
GRA06550
GRA06560
GRA06570
GRA06580
GRA06590
GRA06600
GRA06610
GRA06620
GRA06630
GRA06640
GRA06650

```



```

COMMON /DEF/TEGMX,SENGMX,SENGMN,TARTM,SARTM,TVEL,SVEL
COMMON /SUPEFT/GAMMA,DELTA
ROF=0.0
IF(RANGE.LT.25.) RETURN
IF(IWPN.EQ.2) GO TO 500
IF(RANGE.GT.TEGMX) RETURN
TRTN=TARTM*(1.0+GAMMA*SUPFAC)
DT=TRTN+RANGE/(TVEL+SPEED)
ROF=1.0/DT
RETURN
500 IF(RANGE.GT.SENGMX) RETURN
IF(RANGE.LT.SENGMN) RETURN
SRTM=SARTM*(1.0+GAMMA*SUPFAC)
DT=SRTM+RANGE/(SVEL+SPEED)
ROF=1.0/DT
RETURN
END

```

C

```

FUNCTION SPD(T)
COMMON /ENGR/ SPDMAX,SPDMIN,HTMAX,HTMIN,TTS,TAA,TB,TFF
IF(T.GT.TAA) GO TO 50
SPD=SPDMAX
RETURN
50 IF(T.GT.TB) GO TO 100
SPD=SPDMIN+((TB-T)/TTS)*(SPDMAX-SPDMIN)
RETURN
100 SPD=SPDMIN
RETURN
END

```

C

```

FUNCTION HT(T)
COMMON /ENGR/ SPDMAX,SPDMIN,HTMAX,HTMIN,TTS,TAA,TB,TFF
IF(T.GT.TAA) GO TO 50
HT=HTMAX
RETURN
50 IF(T.GT.TB) GO TO 100
HT=HTMIN+((TB-T)/TTS)*(HTMAX-HTMIN)
RETURN
100 HT=HTMIN
RETURN
END

```

C

```

FUNCTION RNG(T)
COMMON /AMPH/IL(5),WB(2),A(2),B(2),ITE,ISE,RD,WVINT(5),WID,
1TBW,DINIT(2),GAINL,IWSTAT(5)
COMMON /ENGR/ SPDMAX,SPDMIN,HTMAX,HTMIN,TTS,TAA,TB,TFF
IF(T.GT.TAA) GO TO 50

```

GRA06660
 GRA06670
 GRA06680
 GRA06690
 GRA06700
 GRA06710
 GRA06720
 GRA06730
 GRA06740
 GRA06750
 GRA06760
 GRA06770
 GRA06780
 GRA06790
 GRA06800
 GRA06810
 GRA06820
 GRA06830
 GRA06840
 GRA06850
 GRA06860
 GRA06870
 GRA06880
 GRA06890
 GRA06900
 GRA06910
 GRA06920
 GRA06930
 GRA06940
 GRA06950
 GRA06960
 GRA06970
 GRA06980
 GRA06990
 GRA07000
 GRA07010
 GRA07020
 GRA07030
 GRA07040
 GRA07050
 GRA07060
 GRA07070
 GRA07080
 GRA07090
 GRA07100
 GRA07110
 GRA07120
 GRA07130

GRA07140
GRA07150
GRA07160
GRA07170
GRA07180
GRA07190
GRA07200
GRA07210
GRA07220
GRA07230
GRA07240
GRA07250
GRA07260
GRA07270
GRA07280
GRA07290
GRA07300
GRA07310
GRA07320
GRA07330
GRA07340
GRA07350
GRA07360
GRA07370
GRA07380
GRA07390
GRA07400
GRA07410
GRA07420
GRA07430
GRA07440
GRA07450
GRA07460
GRA07470
GRA07480
GRA07490
GRA07500
GRA07510
GRA07520
GRA07530
GRA07540
GRA07550
GRA07560
GRA07570
GRA07580
GRA07590
GRA07600
GRA07610

```

RNG=5000.0-(SPDMAX*T)
RETURN
50 IF(T.GT.TB) GO TO 100
RNG=RD-0.5*(T-TAA)*(SPDMAX+SPD(T))
RETURN
100 RNG=RD-((TB-TAA)/2.0)*(SPDMIN+SPDMAX))-((T-TB)*SPDMIN)
IF(RNG.LT.75.) RNG=0.0
RETURN
END

SUBROUTINE GROUND(GATM)
COMMON /GRP1/ IPRDIR(6), ISECWD(6), MVTDIR(6), X(6), Y(6), SPD(6)
COMMON /GRP2/ TA(2), T1(2), TH(2), TM(2), TF1(2), TF2(2), TF3(2),
1P(2,6), PHH(2,6), PHM(2,6), PKH(2,6), TF(2)
COMMON /GRP3/ NBU, NRU, FL(6), FO(6), NOI(3), XIC(3,200), YIC(3,200),
1IDIR(3,200), AVSP, ISPD
1IUSTAT(6), I1(6), LOST(6,6), VISFRA, VISFRB, SIZETK,
1SIZETW, NT(6), NF(6), SRF, DISMAX,
INLOSC(6,6), VISFR(6,6), AMINTK, RMXTK, RMINTW, RMXTW, OP, TOWER, TNKFR,
IPTT(3,3), RF, POA(6,6), APOA(6,6), LOA(6,6), NA(6), OFL(6), POL(6)
COMMON /GRP4/ TPOL(6), OLDQ(6,6), Q(6,6)
COMMON /HILLS/ XC(100), SX(100), PEAK(100), SY(100), RHD(100)
COMMON /HILLS/ SCALE(100), TWORHO(100), TWOSCL(100), BASE
COMMON /HILLS/ NHILLS
COMMON /COVER/ CX(150), CPEAK(150), CPXX(150), CPYY(150)
COMMON /COVER/ CPXY(150), NCVELS
COMMON /COUNTR/ KH, KHW, KV, KN, KGRS, KELL, KINT
COMMON /GRID/ LST(10,10), NHL(10,10), LISTH(450), KHREP(100), KTREP
COMMON /GRID/ LSTC(10,10), NC(10,10), LISTC(400), KCREP(150)
COMMON /GRP6/ ALPHA(6)
COMMON /GRP7/ XA(6), YA(6), IMOVE(6)
INITIALIZATION.

BL=0.0
RL=0.0
MP=0
PAI=3.14159
ZL=.00001

READ TERRAIN DATA FOR LINE OF SIGHT
CHECK FOR STOCHASTIC OR DETERMINISTIC ATTRITION
ITRIT-ATTRITION MOD 1=DETERMINISTIC
0=STOCHASTIC
IS-SEED NUMBER

```

```

130 READ(9,130) ITRIT,IS
   FORMAT(1,1X,15)
   DO 132 I=1,6
     CALL LRND(1,IS,YRAN,1,1,0)
     ALPHA(I)=(-2.*YRAN+2)+(2.*YRAN+.3)
     WRITE(6,799) YRAN,ALPHA(I)
132 CONTINUE
799 FORMAT(2X,'YRAN,ALPHA',F10.5,2X,F10.5)
C READ IN NUMBER OF ATTACK AND DEFENSE UNITS
C
C READ(9,200) NBU,NRU
200 FORMAT(12,1X,12)
C INITIALIZE WEAPON SIZES
C
C SIZETK=2.5
C SIZETW=2.5
C READ IN EFFECTIVE WEAPON RANGES
C
C READ(9,102) RMINTK,RMXTK,RMINTW,RMXTW
102 FORMAT(F6.1,1X,F6.1,1X,F6.1,1X,F6.1,1X)
C INITIALIZE PM,RF,TOWFR,TNKFR AND NOD
C
C PM=.352
C RF=.5
C TOWFR=.03
C TNKFR=.1
C NOD=2
C DO 101 I=1,NRU
101 NOI(I)=125
   CONTINUE
   K=NRU+1
   L=NRU+NBU
   DO 111 I=1,L
111 I(I)=0
   CONTINUE
C READ IN FORCE LEVELS OF EACH ATTACK UNIT
C
C READ(9,103) {FL(I),I=1,NRU}
103 FORMAT(3(F3.1,1X))
C CHECK FOR TYPE OF ROUTE DETERMINATION
C
C READ(9,106) IRTE,ISPD

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GRA07620
GRA07630
GRA07640
GRA07650
GRA07660
GRA07670
GRA07680
GRA07690
GRA07700
GRA07710
GRA07720
GRA07730
GRA07740
GRA07750
GRA07760
GRA07770
GRA07780
GRA07790
GRA07800
GRA07810
GRA07820
GRA07830
GRA07840
GRA07850
GRA07860
GRA07870
GRA07880
GRA07890
GRA07900
GRA07910
GRA07920
GRA07930
GRA07940
GRA07950
GRA07960
GRA07970
GRA07980
GRA07990
GRA08000
GRA08010
GRA08020
GRA08030
GRA08040
GRA08050
GRA08060
GRA08070
GRA08080
GRA08090

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GRA08109
 GRA08110
 GRA08120
 GRA08130
 GRA08140
 GRA08150
 GRA08160
 GRA08170
 GRA08180
 GRA08190
 GRA08200
 GRA08210
 GRA08220
 GRA08230
 GRA08240
 GRA08250
 GRA08260
 GRA08270
 GRA08280
 GRA08290
 GRA08300
 GRA08310
 GRA08320
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 GRA08340
 GRA08350
 GRA08360
 GRA08370
 GRA08380
 GRA08390
 GRA08400
 GRA08410
 GRA08420
 GRA08430
 GRA08440
 GRA08450
 GRA08460
 GRA08470
 GRA08480
 GRA08490
 GRA08500
 GRA08510
 GRA08520
 GRA08530
 GRA08540
 GRA08550
 GRA08560
 GRA08570

106 FORMAT(11,1X,11)
 IF(IISPD.EQ.1) AVSP=9.0
 IF(IISPD.EQ.1) DST=40.232
 IF(IISPD.EQ.2) AVSP=12.0
 IF(IISPD.EQ.3) DST=53.643
 IF(IISPD.EQ.3) AVSP=15.0
 IF(IISPD.EQ.3) DST=67.053
 IF(IISPD.EQ.4) AVSP=18.0
 IF(IISPD.EQ.4) DST=80.463

C READ IN INITIAL ATTACK UNIT'S LOCATIONS
 C

107 DC 6 I=1,NRU
 READ(9,107) XIC(I,1),YIC(I,1)
 6 FORMAT(F6.1,1X,F6.1)
 2 CONTINUE
 IF(IRTE.EQ.1) GO TO 108
 DO 2 I=1,NRU
 DO 2 J=2,125
 YIC(I,J)=YIC(I,J-1)+DST*(J-1)
 XIC(I,J)=XIC(I,J-1)+DST*(J-1)
 IDIR(I,J)=0
 2 CONTINUE
 GO TO 109

108 CALL ROUTE
 109 SUMRO=0.0
 DO 3 I=1,NRU
 FO(I)=FL(I)
 SUMRO=SUMRO+FO(I)
 X(I)=XIC(I,1)
 Y(I)=YIC(I,1)
 MVDIR(I)=IDIR(I,1)
 SPD(I)=AVSP
 IUSTAT(I)=0
 IPRDIR(I)=IDIR(I,1)
 ISECWD(I)=120
 NF(I)=1
 IF(I)=1
 3 CONTINUE

C READ IN DEFENSE UNIT'S LOCATIONS
 C

104 SUMBO=0.0
 DO 4 I=K,L
 READ(9,104) X(I),Y(I),FL(I),IPRDIR(I),ISECWD(I)
 104 FORMAT(F6.1,1X,F6.1,1X,F3.1,1X,13,1X,13)
 FO(I)=FL(I)
 SUMBO=SUMBO+FO(I)

GRA08580
 GRA08590
 GRA08600
 GRA08610
 GRA08620
 GRA08630
 GRA08640
 GRA08650
 GRA08660
 GRA08670
 GRA08680
 GRA08690
 GRA08700
 GRA08710
 GRA08720
 GRA08730
 GRA08740
 GRA08750
 GRA08760
 GRA08770
 GRA08780
 GRA08790
 GRA08800
 GRA08810
 GRA08820
 GRA08830
 GRA08840
 GRA08850
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 GRA08870
 GRA08880
 GRA08890
 GRA08900
 GRA08910
 GRA08920
 GRA08930
 GRA08940
 GRA08950
 GRA08960
 GRA08970
 GRA08980
 GRA08990
 GRA09000
 GRA09010
 GRA09020
 GRA09030
 GRA09040
 GRA09050

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MVIDIR(I)=0
SPD(I)=0.0
IUSTAT(I)=0
IMOVE(I)=0
4 CONTINUE

C CHECK FOR ALTERNATE DEFENSE POSITIONS AND READ IN IF WANTED
C
      READ(9,400) IALT,BREAK,ITEM
      400 FORMAT(I1,I1X,F6.1,I1X,I2)
      IF(IALT.EQ.1) GO TO 401
      DO 402 I=K,L
      402 READ(9,107) XA(I),YA(I)
      CONTINUE
      401 DELT=10.
      TA(I)=20.
      TI(I)=8.
      TH(I)=8.
      TM(I)=10.
      TF1(I)=1.
      TF2(I)=1.
      TF3(I)=1.
      TA(2)=20.
      TI(2)=8.
      TH(2)=8.
      TM(2)=15.
      TF1(2)=10.
      TF2(2)=12.
      TF3(2)=15.

C READ IN HIT AND KILL PROBABILITIES
C
      DO 5 I=1,2
      514 J=1,6
      READ(9,515) P(I,J),PHM(I,J),PHN(I,J),PKH(I,J)
      515 FORMAT(4(F4.2,I1X))
      CONTINUE
      516 P(I,1)=1.0
      P(I,2)=0.8
      P(I,3)=0.2
      P(I,4)=0.8
      P(I,5)=0.15
      P(I,6)=0.05
      DC 31 I=1,NRU
      31 J=K,L
      NLOSC(I,J)=0
  
```

GRA09060
 GRA09070
 GRA09080
 GRA09090
 GRA09100
 GRA09110
 GRA09120
 GRA09130
 GRA09140
 GRA09150
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 GRA09170
 GRA09180
 GRA09190
 GRA09200
 GRA09210
 GRA09220
 GRA09230
 GRA09240
 GRA09250
 GRA09260
 GRA09270
 GRA09280
 GRA09290
 GRA09300
 GRA09310
 GRA09320
 GRA09330
 GRA09340
 GRA09350
 GRA09360
 GRA09370
 GRA09380
 GRA09390
 GRA09400
 GRA09410
 GRA09420
 GRA09430
 GRA09440
 GRA09450
 GRA09460
 GRA09470
 GRA09480
 GRA09490
 GRA09500
 GRA09510
 GRA09520
 GRA09530

```

    Q(I,J)=1.0
    Q(J,I)=1.0
    VISFR(I,J)=0.0
    VISFR(J,I)=0.0
31  CONTINUE
    IC=1

C  PRINT INITIAL BATTLE INFORMATION
C
    WRITE(6,599)
599  FORMAT(1,1X,'INITIAL GROUND COMBAT INFORMATION')
600  WRITE(6,600)
    FORMAT(1X,'UNIT',7X,'X',8X,'Y',4X,'FORCE LEVEL')
    DO 601 I=1,L
601  WRITE(6,602) I,X(I),Y(I),FL(I)
    FORMAT(1X,13,3X,F7.1,2X,F7.1,7X,F3.1)
    CONTINUE
    IF(I.EQ.1) GO TO 603
    WRITE(6,604)
    FORMAT(1X,'ATTRITION IS STOCHASTIC')
    GO TO 605
603  WRITE(6,606)
    FORMAT(1X,'ATTRITION IS DETERMINISTIC')
606  IF(I.EQ.0) GO TO 607
607  WRITE(6,608)
    FORMAT(1X,'ROUTES DETERMINED BY USER')
608  WRITE(6,609)
    FORMAT(1X,'AVSP')
609  WRITE(6,610)
    FORMAT(1X,'ATTACK VEHICLE SPEED IS',F4.1)
610  WRITE(6,611)
    FORMAT(1X,'BREAKPOINT DISTANCE IS',F6.1)
    IF(I.EQ.0) GO TO 615
    WRITE(6,620)
    FORMAT(1X,'DEFENDER WILL NOT MOVE TO ALTERNATE POSITIONS')
    GO TO 625
615  WRITE(6,630)
    FORMAT(1X,'DEFENDER WILL MOVE TO ALTERNATE POSITIONS')
630  IF(I.EQ.0) GO TO 635
    WRITE(6,631)
    FORMAT(1X,13,3X,F7.1,2X,F7.1)
    DO 635 I=1,K
635  CONTINUE
    WRITE(6,645)
    FORMAT(1X,4X,'ATK KILL PROBABILITIES',1X,'RANGE',4X,'P',
    14X,'PHM',3X,'PHM',3X,'PKH')
    DO 650 I=1,6
650  CONTINUE
    WRITE(6,655)
    FORMAT(1X,14,4(2X,F4.2))
  
```

```

        IRAN=IRAN+500
650  CONTINUE
        IRAN=500
        WRITE(6,660) DEF. KILL PROBABILITIES'/1X,'RANGE',4X,'P',
660  FORMAT(14X,'PHH',3X,'PHM',3X,'PKH')
        DO 665 I=1,6
        WRITE(6,665) IRAN,P(2,I),PHH(2,I),PHM(2,I),PKH(2,I)
665  CONTINUE
        IRAN=IRAN+500
        WRITE(6,670)
670  FORMAT(11,10X,'BATTLE BEGINS',/)
        C  UPDATE LOCATION OF RED UNITS.
        C
        DISMAX=5000.0
        DO 9 I=1,NRU
        IF(IUSTAT(I).EQ.2) GOTO 9
        IF(IUSTAT(I).EQ.0) GOTO 76
        NF(I)=NF(I)+1
        IF(NF(I).LT.NOD) GOTO 9
        NF(I)=1
        DO 11 J=1,NRU
        IF(J.EQ.1) GO TO 11
        IF(IUSTAT(J).EQ.2) GO TO 11
        DIST=X(I)-X(J)
        IF(DIST.GT.DISMAX) GO TO 9
        11  CONTINUE
        II(I)=II(I)+1
        K7=II(I)
        X(I)=XIC(I,K7)
        Y(I)=YIC(I,K7)
        MVTDIR(I)=IDIR(I,K7)
        IPRDIR(I)=IDIR(I,K7)
        WRITE(6,666) I,X(I),Y(I),MVTDIR(I),IPRDIR(I)
        666  FORMAT(1X,13,1X,F10.5,2X,F10.5,2X,F10.5,2X,F10.5,/)
        C  CONTINUE
        C
        C  LINE--OF-SIGHT CHECK BETWEEN UNITS AND TARGETS SELECTION
        DO 17 J=K,L
        NT(J)=0
        17  CONTINUE
        DO 12 I=1,NRU
        NT(I)=0
        IF(IUSTAT(I).EQ.2) GOTO 12
        DO 16 J=K,L
        IF(IUSTAT(J).EQ.2.OR.IUSTAT(J).EQ.3) GO TO 16
        XX1=X(I)

```

GRA09540
 GRA09550
 GRA09560
 GRA09570
 GRA09580
 GRA09590
 GRA09600
 GRA09610
 GRA09620
 GRA09630
 GRA09640
 GRA09650
 GRA09660
 GRA09670
 GRA09680
 GRA09690
 GRA09700
 GRA09710
 GRA09720
 GRA09730
 GRA09740
 GRA09750
 GRA09760
 GRA09770
 GRA09780
 GRA09790
 GRA09800
 GRA09810
 GRA09820
 GRA09830
 GRA09840
 GRA09850
 GRA09860
 GRA09870
 GRA09880
 GRA09890
 GRA09900
 GRA09910
 GRA09920
 GRA09930
 GRA09940
 GRA09950
 GRA09960
 GRA09970
 GRA09980
 GRA09990
 GRA10000
 GRA10010

```

133      YY1=Y(I)
        CALL ELEV(XX1,YY1,TMACI)
        XX2=X(J)
        YY2=Y(J)
        CALL ELEV(XX2,YY2,TMACJ)
        LATOB=1
        LBTOA=1
        WRITE(6,675) XX1,YY1,TMACI,XX2,YY2,TMACJ
        C 675  FORMAT(1X,5PRELOS,1X,6(F10.5,1X))
        CALL LOS(XX1,YY1,TMACI,0.0,SIZEWK,XX2,YY2,TMACJ,0.0,SIZEW,
        1  VISFR(I,J)=VISFRA
        VISFR(J,I)=VISFRB
        IF(VISFRA.GT.ZL) GOTO 18
        LOST(I,J)=0
        LOST(J,I)=0
        NLOSC(I,J)=NLOSC(I,J)+1
        NLOSC(J,I)=NLOSC(I,J)
        GOTO 16
18      LOST(I,J)=1
        LOST(J,I)=1
        NLOSC(I,J)=0
        NLOSC(J,I)=0
        RANGE=SQRT((X(I)-X(J))**2+(Y(I)-Y(J))**2)
        IF(RANGE.LT.RMINTK.OR.RANGE.GT.RMXTK) GOTO 20
        IUSTAT(I)=1
        IUSTAT(J)=1
        NT(I)=NT(I)+1
        NT(J)=NT(J)+1
        LOT(I,M)=J
        RCT(I,M)=RANGE
        IF(M.EQ.1) GOTO 20
        CALL SORT(I,M)
20      IF(RANGE.LT.RMINTK.OR.RANGE.GT.RMXTK) GOTO 16
        IUSTAT(I)=1
        IUSTAT(J)=1
        NT(I)=NT(I)+1
        NT(J)=NT(J)+1
        M=NT(J)
        LOT(J,M)=I
        RCT(J,M)=RANGE
        IF(M.EQ.1) GOTO 16
        CALL SORT(J,M)
16      CONTINUE
12      DO 25 I=1,NRU
        IF(IUSTAT(I).EQ.2) GOTO 25
        IF(NT(I).NE.0) GOTO 25
        IUSTAT(I)=0

```

```

GRA10020
GRA10030
GRA10040
GRA10050
GRA10060
GRA10070
GRA10080
GRA10090
GRA10100
GRA10110
GRA10120
GRA10130
GRA10140
GRA10150
GRA10160
GRA10170
GRA10180
GRA10190
GRA10200
GRA10210
GRA10220
GRA10230
GRA10240
GRA10250
GRA10260
GRA10270
GRA10280
GRA10290
GRA10300
GRA10310
GRA10320
GRA10330
GRA10340
GRA10350
GRA10360
GRA10370
GRA10380
GRA10390
GRA10400
GRA10410
GRA10420
GRA10430
GRA10440
GRA10450
GRA10460
GRA10470
GRA10480
GRA10490

```


GRA10500
GRA10510
GRA10520
GRA10530
GRA10540
GRA10550
GRA10560
GRA10570
GRA10580
GRA10590
GRA10600
GRA10610
GRA10620
GRA10630
GRA10640
GRA10650
GRA10660
GRA10670
GRA10680
GRA10690
GRA10700
GRA10710
GRA10720
GRA10730
GRA10740
GRA10750
GRA10760
GRA10770
GRA10780
GRA10790
GRA10800
GRA10810
GRA10820
GRA10830
GRA10840
GRA10850
GRA10860
GRA10870
GRA10880
GRA10890
GRA10900
GRA10910
GRA10920
GRA10930
GRA10940
GRA10950
GRA10960
GRA10970

```

NF(I)=0
25 CONTINUE
  DO 79 J=K,L
    IF(IUSTAT(J).EQ.2.OR.IUSTAT(J).EQ.3) GO TO 79
    IF(NT(J).EQ.0) IUSTAT(J)=0
79 CONTINUE

C
C  UPDATE OF THE ACCUMULATED DETECTION PROBABILITIES.
C
  IAA=1
  IBB=NRU
  ICC=K
  IDD=L
  FR=TOWFR
  OP=PM
  DO 345 I=1,6
345 CONTINUE
  DO 14 I=IAA,IBB
37 IF(IUSTAT(I).EQ.2.OR.IUSTAT(I).EQ.3) GO TO 14
  DO 19 J=ICC,IDD
    PROP=0.0
    IF(IUSTAT(J).EQ.2.OR.IUSTAT(J).EQ.3) GO TO 19
    OLDQ(I,J)=Q(I,J)
    IF(LOST(I,J).EQ.0) GO TO 15
    IF(NT(I).GT.0) GO TO 22
    PCTVI=VISFR(J,I)
    CALL LAMDA(I,J,PCTVIS,DETRAT,PSUBK)
    QV=EXP(-(FL(I)*DETRAT*OP*DELT*FL(J)))
    IF(NT(J).GT.0) GO TO 23
    Q(I,J)=Q(I,J)*QV
    GO TO 19
23 QP=(1.0-PSUBK)*((FR*DELT*FL(I)*FL(J))
  Q(I,J)=Q(I,J)*(QV+QP-QV*QP)
  GO TO 19
22 N5=NT(I)
  DO 24 I1=1,N5
    K1=LOTT(I1)
    ANG1=ATAN2(Y(K1)-Y(I),X(K1)-X(I))
    ANG2=ATAN2(Y(J)-Y(I),X(J)-X(I))
    IF((ANG1-ANG2).GE.0.0) GO TO 77
    IF(ANG2-LT.0.0) GO TO 32
    ANG=2*PAI+ANG1-ANG2
    GO TO 35
32 ANG=2*PAI+ANG2-ANG1
35 IF(ANG.GT.PAI) ANG=2*PAI-ANG
  GO TO 33
77 ANG=ABS(ANG2-ANG1)
33 AA=15.0*PAI/180.0

```

GRA10980
GRA10990
GRA11000
GRA11010
GRA11020
GRA11030
GRA11040
GRA11050
GRA11060
GRA11070
GRA11080
GRA11090
GRA11100
GRA11110
GRA11120
GRA11130
GRA11140
GRA11150
GRA11160
GRA11170
GRA11180
GRA11190
GRA11200
GRA11210
GRA11220
GRA11230
GRA11240
GRA11250
GRA11260
GRA11270
GRA11280
GRA11290
GRA11300
GRA11310
GRA11320
GRA11330
GRA11340
GRA11350
GRA11360
GRA11370
GRA11380
GRA11390
GRA11400
GRA11410
GRA11420
GRA11430
GRA11440
GRA11450

```

IF(ANG.GT.AA) GOTO 24
PROP=PROP+PTT(I1,N5)
CONTINUE
24 IF(PROP.EQ.0.0) GOTO 34
IF(NT(J).GT.0) GOTO 36
CALL LAMDA(I,J,PCTVIS,DETRAT,PSUBK)
DETRAT=DETRAT*RF
QV=EXP(-(FL(I)*PROP*DETRAT*DELT*FL(J)))
Q(I,J)=Q(I,J)*QV
GOTO 19
36 Q(I,J)=0.0
GOTO 19
34 IF(IAA.EQ.1) GOTO 19
Q(I,J)=1.0
GOTO 19
15 IF(NLOSC(I,J).LE.3) GOTO 19
Q(I,J)=1.0
CONTINUE
14 CONTINUE
IF(IAA.EQ.K) GOTO 38
FR=TNKFR
IAA=K
I88=L
ICC=1
IDD=NRU
OP=1.0
GOTO 37

FIRE ALLOCATION.

38 DO 28 I=1,L
28 NA(I)=0
DO 26 I=1,L
IF(IUSTAT(I).EQ.2.OR.IUSTAT(I).EQ.3) GO TO 26
IF(NT(I).EQ.0) GOTO 26
DC 27 J=1,3
APOA(I,J)=0.0
CONTINUE
27 IF(NT(I).EQ.1) GOTO 78
IF(NT(I).EQ.2) GOTO 29
NOT=3
MM1=LOT(I,1)
MM2=LOT(I,2)
MM3=LOT(I,3)
PROB=(1.0-Q(I,MM1))*Q(I,MM2)*Q(I,MM3)
APOA(I,1)=APOA(I,1)+PTT(I,1)*PROB
PROB=Q(I,MM1)*(1.0-Q(I,MM2))*Q(I,MM3)
APOA(I,2)=APOA(I,2)+PTT(I,1)*PROB

```

CC

GRA11460
 GRA11470
 GRA11480
 GRA11490
 GRA11500
 GRA11510
 GRA11520
 GRA11530
 GRA11540
 GRA11550
 GRA11560
 GRA11570
 GRA11580
 GRA11590
 GRA11600
 GRA11610
 GRA11620
 GRA11630
 GRA11640
 GRA11650
 GRA11660
 GRA11670
 GRA11680
 GRA11690
 GRA11700
 GRA11710
 GRA11720
 GRA11730
 GRA11740
 GRA11750
 GRA11760
 GRA11770
 GRA11780
 GRA11790
 GRA11800
 GRA11810
 GRA11820
 GRA11830
 GRA11840
 GRA11850
 GRA11860
 GRA11870
 GRA11880
 GRA11890
 GRA11900
 GRA11910
 GRA11920
 GRA11930

```

PROB=Q(I,MM1)*Q(I,MM2)*(1.0-Q(I,MM3))
APOA(I,3)=APOA(I,3)+PTT(1,1)*PROB
PROB=((1.0-Q(I,MM1))*Q(I,MM2))*Q(I,MM3)
APOA(I,1)=APOA(I,1)+PTT(1,2)*PROB
APOA(I,2)=APOA(I,2)+PTT(2,2)*PROB
PROB=((1.0-Q(I,MM1))*Q(I,MM2))*Q(I,MM3)
APOA(I,1)=APOA(I,1)+PTT(1,2)*PROB
APOA(I,3)=APOA(I,3)+PTT(2,2)*PROB
PROB=((1.0-Q(I,MM1))*Q(I,MM2))*Q(I,MM3)
APOA(I,1)=APOA(I,1)+PTT(1,2)*PROB
APOA(I,3)=APOA(I,3)+PTT(2,2)*PROB
PROB=((1.0-Q(I,MM1))*Q(I,MM2))*Q(I,MM3)
APOA(I,1)=APOA(I,1)+PTT(1,2)*PROB
APOA(I,3)=APOA(I,3)+PTT(2,2)*PROB
APOA(I,3)=APOA(I,3)+PTT(3,3)*PROB
DO 44 J=1,NOT
KK=LOT(I,J)
NA(KK)=NA(KK)+1
IN=NA(KK)
LOAD(KK,IN)=I
POA(KK,IN)=APOA(I,J)
44 CONTINUE
29 GOTO 26
NOT=2
MM1=LOT(I,1)
MM2=LOT(I,2)
PROB=((1.0-Q(I,MM1))*Q(I,MM2))*PROB
APOA(I,1)=APOA(I,1)+PTT(1,1)*PROB
PROB=((1.0-Q(I,MM1))*Q(I,MM2))*PROB
APOA(I,2)=APOA(I,2)+PTT(1,1)*PROB
PROB=((1.0-Q(I,MM1))*Q(I,MM2))*PROB
APOA(I,1)=APOA(I,1)+PTT(1,2)*PROB
APOA(I,2)=APOA(I,2)+PTT(2,2)*PROB
GOTO 30
78 NOT=1
MM1=LOT(I,1)
PROB=((1.0-Q(I,MM1))*Q(I,MM2))*PROB
APOA(I,1)=APOA(I,1)+PTT(1,1)*PROB
GOTO 30
26 CONTINUE
ATTRITION.
SUMR=0.0
SUMB=0.0
DO 40 I=1,L
IF(IUSTAT(I).EQ.2.OR.IUSTAT(I).EQ.3) GO TO 40
  
```

C
 C
 C

GRAI1940
GRAI1950
GRAI1960
GRAI1970
GRAI1980
GRAI1990
GRAI2000
GRAI2010
GRAI2020
GRAI2030
GRAI2040
GRAI2050
GRAI2060
GRAI2070
GRAI2080
GRAI2090
GRAI2100
GRAI2110
GRAI2120
GRAI2130
GRAI2140
GRAI2150
GRAI2160
GRAI2170
GRAI2180
GRAI2190
GRAI2200
GRAI2210
GRAI2220
GRAI2230
GRAI2240
GRAI2250
GRAI2260
GRAI2270
GRAI2280
GRAI2290
GRAI2300
GRAI2310
GRAI2320
GRAI2330
GRAI2340
GRAI2350
GRAI2360
GRAI2370
GRAI2380
GRAI2390
GRAI2400
GRAI2410

```

M6=NA(I)
SUM=0.0
IF(M6.EQ.0) GOTO 47
DO 41 J=1,M6
M7=LOA(I,J)
IF(M7.LI.K) GOTO 42
ITYPE=2
GOTO 43
42 ITYPE=1
43 RANGE=SQRT((X(I)-X(M7))**2+(Y(I)-Y(M7))**2)
IF (ITRIT.EQ.1) GO TO 131
CALL STOCH(ITYPE,RANGE,AJI)
GO TO 5000
131 CALL ETK(ITYPE,RANGE,T)
AJI=1.0/T
SUM=SUM+AJI*FL(M7)*POA(I,J)*DELT
5000 CONTINUE
41 OFL(I)=FL(I)
47 FL(I)=FL(I)-SUM
IF(FL(I).GT.ZL) GOTO 46
FL(I)=0.0
IUSTAT(I)=2
IF(I.LT.K) GOTO 60
46 SUMB=SUMB+FL(I)
TPOL(I)=(FO(I)-FL(I))/FO(I)
GO TO 40
60 SUMR=SUMR+FL(I)
TPOL(I)=(FO(I)-FL(I))/FO(I)
40 CONTINUE

PRINT AND CHECK FOR BATTLE DETERMINATION.

C
C
C
ITIME=IC*10
DO 57 I=K,L
IF(IUSTAT(I).EQ.2) GO TO 57
DO 58 J=1,NRU
IF(IUSTAT(J).EQ.2) GO TO 58
CHECK=X(I)-X(J)
AVD=SQRT((X(I)-X(J))**2+(Y(I)-Y(J))**2)
IF(AVD.LI.BREAK.OR.CHECK.LI.50.) GO TO 250
58 CONTINUE
57 CONTINUE
GO TO 99
C
C
C
COMPLETE ATTACK UNIT'S MOVE
C
C
250 DO 251 I=K,L

```

GRA12420
GRA12430
GRA12440
GRA12450
GRA12460
GRA12470
GRA12480
GRA12490
GRA12500
GRA12510
GRA12520
GRA12530
GRA12540
GRA12550
GRA12560
GRA12570
GRA12580
GRA12590
GRA12600
GRA12610
GRA12620
GRA12630
GRA12640
GRA12650
GRA12660
GRA12670
GRA12680
GRA12690
GRA12700
GRA12710
GRA12720
GRA12730
GRA12740
GRA12750
GRA12760
GRA12770
GRA12780
GRA12790
GRA12800
GRA12810
GRA12820
GRA12830
GRA12840
GRA12850
GRA12860
GRA12870
GRA12880
GRA12890

```

IF(IALT.EQ.1.OR.IMOVE(I).EQ.ITEM) GO TO 6000
IF(IUSTAT(I).EQ.0) IUSTAT(I)=3
IMOVE(I)=IMOVE(I)+1
IF(IMOVE(I).LT.ITEM) GO TO 251
X(I)=XA(I)
Y(I)=YA(I)
IF(IUSTAT(I).EQ.3) IUSTAT(I)=0
251 CONTINUE
99 IITIME=IITIME+IFIX(GATM)
112 WRITE(6,112) IITIME
112 FORMAT(///IX,TIME=,I4,IX,SECONDS'//)
113 WRITE(6,113)
113 FORMAT(IX,UNIT=,5X,X,8X,Y,5X,FORCE LEVEL',2X,STATUS',
12X,LOST-PCT',2X,TARGETS,}
DO 59 I=1,L
N6=NT(I)
IF(N6.NE.0) GO TO 48
WRITE(6,264) I,X(I),Y(I),FL(I),IUSTAT(I),TPOL(I)
264 FORMAT(3X,I1,3X,F7.1,2X,F7.1,6X,F3.1,9X,I1,6X,F5.3)
48 GO TO 59
48 WRITE(6,114) I,X(I),Y(I),FL(I),IUSTAT(I),TPOL(I),
1(LOTT(I),J),J=1,N6)
114 FORMAT(3X,I1,3X,F7.1,2X,F7.1,6X,F3.1,9X,I1,6X,F5.3,3(11,1X))
59 CONTINUE

CHECK FOR BATTLE TERMINATION.

IOT=0
DO 53 I=1,NRU
IF(FL(I).EQ.0.0) GOTO 53
IOT=1
53 CONTINUE
IF(IOT.EQ.1) GOTO 54
WRITE(6,117)
117 FORMAT(IX,ATTACK FORCE IS ELIMINATED. END OF BATTLE.
54 GOTO 66
54 IOT=0
DO 55 I=K,L
IF(FL(I).EQ.0.0) GOTO 55
IOT=1
55 CONTINUE
IF(IOT.EQ.1) GOTO 65
WRITE(6,118)
118 FORMAT(IX,DEFENSE FORCE IS ELIMINATED. END OF BATTLE.
6000 GOTO 66
6000 WRITE(6,119)
119 FORMAT(IX,DISTANCE BETWEEN FORCES IS TOO CLOSE. END OF BATTLE
1,1)

```

GRA12900
GRA12910
GRA12920
GRA12930
GRA12940
GRA12950
GRA12960
GRA12970
GRA12980
GRA12990
GRA13000
GRA13010
GRA13020
GRA13030
GRA13040
GRA13050
GRA13060
GRA13070
GRA13080
GRA13090
GRA13100
GRA13110
GRA13120
GRA13130
GRA13140
GRA13150
GRA13160
GRA13170
GRA13180
GRA13190
GRA13200
GRA13210
GRA13220
GRA13230
GRA13240
GRA13250
GRA13260
GRA13270
GRA13280
GRA13290
GRA13300
GRA13310
GRA13320
GRA13330
GRA13340
GRA13350
GRA13360
GRA13370

```

65  GO TO 66
    IC=IC+1
66  GO TO 67
    RETURN
    END

C      SUBROUTINE SETUP
C      SUBROUTINE SETUP IS USED TO READ IN THE TERRAIN DATA AND
C      CREATE PARAMETRIC TERRAIN. THIS TERRAIN DATA WILL BE USED
C      WHEN COMPUTING LINE-OF-SIGHT BETWEEN TARGETS AND OBSERVERS
C      AS WELL AS PROVIDING A GRID SYSTEM FOR UNIT LOCATIONS AND
C      MOVEMENT.
COMMON /HILLS/ XC(100),YC(100),PEAK(100),ANGH(100),SPRD(100)
COMMON /HILLS/ ECC(100),PXX(100),PY(100),PXY(100),BASE
COMMON /HILLS/ NHILLS
COMMON /COVER/ CX(150),CYC(150),CPEAK(150),CPXX(150),CPYY(150)
COMMON /COVER/ CPXY(150),NCVELS
COMMON /COUNTR/KH KHW,KV,KN,KGRS,KELL,KINT
COMMON /GRID/ LST(5,4),NHL(5,4),LISTH(150),KHREP(150),KTREP
COMMON /GRID/ LSTC(5,4),NC(5,4),LISTC(400),KCREP(150)
PAI=3.14159
L=5
READ(L,7) NHILLS
READ(L,47) BASE
FORMAT(F10.4)
FORMAT(I6)
FORMAT(6F10.3)
DO 50 I=1,NHILLS
  READ(L,17) XC(I),YC(I),PEAK(I),ANGH(I),SPRD(I),ECC(I)
  CONTINUE
READ(L,37) LST
READ(L,37) NHL
READ(L,7) NHTOT
READ(L,37) (LISTH(I),I=1,NHTOT)
FORMAT(I6)
DO 100 I=1,NHILLS
  ANGLE=ANGH(I)*PAI/180.
  SANG=SIN(ANGLE)
  CANG=COS(ANGLE)
  A=PEAK(I)/(PEAK(I)-50.)
  A=A*LOG(A)
  B=A*ECC(I)**2
  SSPD=SPRD(I)**2
  PXX(I)=-(A*CANG*CANG+B*SANG*SANG)/SSPD
  PY(I)=-(A*SANG*SANG+B*CANG*CANG)/SSPD
  PXY(I)=(2.*SANG*CANG*(B-A))/SSPD
  KHREP(I)=-2.147483600

```

GRA13380
 GRA13390
 GRA13400
 GRA13410
 GRA13420
 GRA13430
 GRA13440
 GRA13450
 GRA13460
 GRA13470
 GRA13480
 GRA13490
 GRA13500
 GRA13510
 GRA13520
 GRA13530
 GRA13540
 GRA13550
 GRA13560
 GRA13570
 GRA13580
 GRA13590
 GRA13600
 GRA13610
 GRA13620
 GRA13630
 GRA13640
 GRA13650
 GRA13660
 GRA13670
 GRA13680
 GRA13690
 GRA13700
 GRA13710
 GRA13720
 GRA13730
 GRA13740
 GRA13750
 GRA13760
 GRA13770
 GRA13780
 GRA13790
 GRA13800
 GRA13810
 GRA13820
 GRA13830
 GRA13840
 GRA13850

C ALL VALUES NOW IN METERS ON 0 -- 10,000 GRID
 100 CONTINUE
 READ(L,7) NCVELS
 IF(NCVELS.EQ.0) GO TO 75
 DO 60 I=1,NCVELS
 READ(L,27)CXC(I),CYC(I),CPEAK(I),CPXX(I),CPYY(I),CPXY(I)
 FORMAT(3F10.4,3E13.7)
 KCREP(I)=-2147483600
 CONTINUE
 READ(L,37)LSTC
 READ(L,37)NC
 READ(L,7)NCIOT
 READ(L,37)(LISTC(I),I=1,NCIOT)
 75 KIREP=-2147483600
 KH=0
 KHW=0
 KV=0
 KN=0
 KGRS=0
 KELL=0
 KINT=0
 RETURN
 END

C SUBROUTINE ROUTE
 C SUBROUTINE ROUTE COMPUTES THE ROUTE OF EACH ATTACKING UNIT
 C WHEN THE USER HAS SELECTED THE OPTION OF INPUTTING ATTACKER
 C ROUTES. IT CALCULATES THE COORDINATES OF EACH INTERVAL END POINT
 C ALONG THE ROUTE, MAKING EACH INTERVAL LENGTH (DISTANCE MOVED DURING
 C A 10 SECOND TIME STEP) THE SAME. THE INTERVAL LENGTH IS DETERMINED
 C BY THE SPEED THE USER HAS SELECTED AND INPUTED FOR THE CURRENT
 C BATTLE.
 C
 C COMMON /GRP3/ NBU,NRU,FL(6),FO(6),NOI(3),XIC(3,200),YIC(3,200),
 C ICDIR(3,200),AVSP,ISPD,
 C IUSTAT(6),I(6),LOST(6),VISFRA,VISFRB,SIZEK,
 C ISIZETW,NT(6),NF(6),SRF,DISMAX,
 C INLOSC(6,6),VISFR(6,6),RMINTK,RMXTK,RMINTW,RMXTW,OP,TOWER,TNKFR,
 C IPTTT(3,3),RF,POA(6,6),APOA(6,6),LOA(6,6),NA(6),OFL(6),POL(6)
 C DIMENSION XLOC(3,20),YLOC(3,20),N(3)
 C IF(ISPD.EQ.4) DST=80.463
 C IF(ISPD.EQ.3) DST=67.053
 C IF(ISPD.EQ.2) DST=53.643
 C IF(ISPD.EQ.1) DST=40.232
 C LN=9
 C DO 300 I=1,NRU
 C READ(LN,15) N(I)

GRA13860
 GRA13870
 GRA13880
 GRA13890
 GRA13900
 GRA13910
 GRA13920
 GRA13930
 GRA13940
 GRA13950
 GRA13960
 GRA13970
 GRA13980
 GRA13990
 GRA14000
 GRA14010
 GRA14020
 GRA14030
 GRA14040
 GRA14050
 GRA14060
 GRA14070
 GRA14080
 GRA14090
 GRA14100
 GRA14110
 GRA14120
 GRA14130
 GRA14140
 GRA14150
 GRA14160
 GRA14170
 GRA14180
 GRA14190
 GRA14200
 GRA14210
 GRA14220
 GRA14230
 GRA14240
 GRA14250
 GRA14260
 GRA14270
 GRA14280
 GRA14290
 GRA14300
 GRA14310
 GRA14320
 GRA14330

```

15  FORMAT(I2)
    NL=N(I)+1
    DO 200 IN=2,NL
      READ(LN,201) XLN,XLOC,YLOC
201  FORMAT(F6.1,IX,F6.1)
      XLOC(I,IN)=XLN
      YLOC(I,IN)=YLOC
200  CONTINUE
      XLOC(I,1)=XIC(I,1)
      YLOC(I,1)=YIC(I,1)
      IDIR(I,1)=0
      NL=N(I)
      NUM=2
      DC 305 J=1,NL
      XL=XLOC(I,J+1)-XLOC(I,J)
      YL=YLOC(I,J+1)-YLOC(I,J)
      DIST=SQRT(XL**2+YL**2)
      Y=ABS(YL)
      Z=Y/XL
      ANGL=ATAN(Z)
      DEG=ANGL*57.2958
      IF(J.EQ.1) GO TO 320
      XLN=(DIST-EXTRA)*COS(ANGL)
      DIST=(DIST+EXTRA)-DIST
      YLN=(DIST-EXTRA)*SIN(ANGL)
      XIC(I,NUM)=XIC(I,NUM-1)+XLN+XLE
      IF(YL.GT.0.) GO TO 325
      YLN=-YLN
325  YIC(I,NUM)=YIC(I,NUM-1)+YLN+YLE
      IF(YL.GT.0.) GO TO 340
      IDIR(I,NUM)=-IFIX(DEG)
      GO TO 341
      IDIR(I,NUM)=IFIX(DEG)
340  NUM=NUM+1
341  XLN=DIST*COS(ANGL)
320  YLN=DIST*SIN(ANGL)
      IF(YL.GT.0.) GO TO 310
      YLN=-YLN
310  IF(DIST.LT.DST) GO TO 315
      XIC(I,NUM)=XIC(I,NUM-1)+XLN
      YIC(I,NUM)=YIC(I,NUM-1)+YLN
      IF(YL.GT.0.) GO TO 342
      IDIR(I,NUM)=-IFIX(DEG)
      GO TO 343
      IDIR(I,NUM)=IFIX(DEG)
342  DIST=DIST-DST
343  NUM=NUM+1
      GO TO 310
  
```


GRA14340
 GRA14350
 GRA14360
 GRA14370
 GRA14380
 GRA14390
 GRA14400
 GRA14410
 GRA14420
 GRA14430
 GRA14440
 GRA14450
 GRA14460
 GRA14470
 GRA14480
 GRA14490
 GRA14500
 GRA14510
 GRA14520
 GRA14530
 GRA14540
 GRA14550
 GRA14560
 GRA14570
 GRA14580
 GRA14590
 GRA14600
 GRA14610
 GRA14620
 GRA14630
 GRA14640
 GRA14650
 GRA14660
 GRA14670
 GRA14680
 GRA14690
 GRA14700
 GRA14710
 GRA14720
 GRA14730
 GRA14740
 GRA14750
 GRA14760
 GRA14770
 GRA14780
 GRA14790
 GRA14800
 GRA14810

```

315  EXTRA=DIST
      XLE=EXTRA*COS(ANGL)
      YLE=EXTRA*SIN(ANGL)
      IF(YL.GT.O.) GO TO 305
305  CONTINUE
300  RETURN
      END
C
C      SUBROUTINE LAMDA(I,J,PCTVIS,DETRAT,PK)
C
C      SUBROUTINE LAMDA IN CONJUNCTION WITH THE LOS ROUTINE COMPUTES
C      THE DETECTION RATE(DETRAT) OF TARGET J BY THE OBSERVER I GIVEN
C      THE PERCENT OF TARGET VISIBLE (PCTVIS) TO THE OBSERVER.
C
      COMMON /GRP1/ IPRDIR(6), ISECWD(6), MVTDIR(6), X(6), Y(6), SPD(6)
      TCFAC1=1.0
      ZEROL=0.00001
      PAI=3.14159
      D=1/SECWD(1)*PAI/180.0/2.0
      B88=(1.0/2.0*(SIN(0)-0*COS(0)))
      IF(ABS(B88).LT.ZEROL) B88=0.0
      AAA=(-B88)*COS(0)
      IF(ABS(AAA).LT.ZEROL) AAA=0.0
      OTANG=ATAN2((Y(J)-Y(I)),(X(J)-X(I)))
      IF(OTANG.LT.-PAI/2.AND.OTANG.GT.-PAI) OTANG=2*PAI+OTANG
      PD=IPRDIR(1)*PAI/180.0
      IF(IPD*OTANG).GE.0.0) GO TO 1
      IF(PD.LT.0.0) GO TO 9
      ANGLE=2*PAI+OTANG-PD
      GO TO 10
9     ANGLE=2*PAI+PD-OTANG
10    IF(ANGLE.GT.PAI) ANGLE=2*PAI-ANGLE
1     GO TO 2
2     ANGLE=ABS(PD-OTANG)
      IF(ANGLE.GT.O) GO TO 3
      DUP=PD+D
      DLOW=PD-D
      ANGLFT=OTANG+(15.0*PAI/180.)
      IF(ANGLFT.GT.DUP) ANGLFT=DUP
      ANGLRT=OTANG-(15.0*PAI/180.)
      IF(ANGLRT.LT.DLOW) ANGLRT=DLOW
      PK=B88*ABS(ABS(SIN(ANGLFT))-ABS(SIN(ANGLRT)))+AAA*(ANGLFT-
1     ANGLRT)
      IF(PK.LT.0.0) GO TO 3
      IF(PK.GT.1.0) GO TO 5
      GO TO 8
  
```

GRA14820
 GRA14830
 GRA14840
 GRA14850
 GRA14860
 GRA14870
 GRA14880
 GRA14890
 GRA14900
 GRA14910
 GRA14920
 GRA14930
 GRA14940
 GRA14950
 GRA14960
 GRA14970
 GRA14980
 GRA14990
 GRA15000
 GRA15010
 GRA15020
 GRA15030
 GRA15040
 GRA15050
 GRA15060
 GRA15070
 GRA15080
 GRA15090
 GRA15100
 GRA15110
 GRA15120
 GRA15130
 GRA15140
 GRA15150
 GRA15160
 GRA15170
 GRA15180
 GRA15190
 GRA15200
 GRA15210
 GRA15220
 GRA15230
 GRA15240
 GRA15250
 GRA15260
 GRA15270
 GRA15280
 GRA15290

```

3 PK=0.0
  DETRAT=0.0
  GOTO 6
5 PK=1.0
8 RANGE=SQRT((X(J)-X(I))**2+(Y(J)-Y(I))**2)
  RR=0.001*RANGE/PC TVIS
  TOANG=ATAN2((Y(I)-Y(J)),(X(I)-X(J)))
  AD=MVTDIR(J)*PAI/180.0
  HORVEL=ABS(SPD(J)*SIN(TOANG-AD))
  HCRVEL=HORVEL*1609.3/3600.0
  DENOM=1.453+TCFACT*(0.5978+2.188*(RR**2)-0.5038*HORVEL)
  IF(DENOM.LE.ZEROL) DENOM=ZEROL
  DETRAT=0.003+1.088/DENOM
  DETRAT=DETRAT*PK
6 RETURN
  END

C SUBROUTINE ELEVIX,Y,TMAC)
C
C SUBROUTINE LEV DETERMINES THE TERRAIN ELEVATION FOR A GIVEN
C SET OF X, Y COORDINATES. THIS FUNCTION IS USED IN CONJUNCTION
C WITH THE LOS SUBROUTINE IN COMPUTING LINE-OF-SIGHT BETWEEN
C OBSERVER AND TARGET.
C
COMMON /HILLS/ XC(100),YC(100),PEAK(100),ANGH(100),SPRD(100)
COMMON /HILLS/ ECC(100),PXX(100),PY(100),PXY(100),BASE
COMMON /HILLS/ NHILLS
COMMON /GRID/ LST(5,4),NHL(5,4),LISTH(150),KHREP(150),KTRP
COMMON /GRID/ LSTC(5,4),NC(5,4),LISTC(400),KCREP(150)
DATA GSIZE/1000./
C FUNCTION TO COMPUTE TERRAIN ELEVATION FOR GIVEN X, Y COORDINATES.
ZMAX=BASE
IX=1+IFIX(X/GSIZE)
IY=1+IFIX(Y/GSIZE)
IF(NHL(IX,IY).EQ.0) GO TO 150
LS=LST(IX,IY)
LEND=LS+NHL(IX,IY)-1
DO 100 L=LS,LEND
  I=LISTH(L)
  QX=X-XC(I)
  QY=Y-YC(I)
  QXSQ=QX*QX
  QYSQ=QY*QY
  QXY=QX*QY
  FACTOR=PXX(I)*QXSQ+PYY(I)*QYSQ+PXY(I)*QXY
  IF(FACTOR.LT.-3.) GO TO 100
  HT=PEAK(I)*EXP(FACTOR)
  IF(HT.LE.ZMAX) GO TO 100
  
```

GRA15300
GRA15310
GRA15320
GRA15330
GRA15340
GRA15350
GRA15360
GRA15370
GRA15380
GRA15390
GRA15400
GRA15410
GRA15420
GRA15430
GRA15440
GRA15450
GRA15460
GRA15470
GRA15480
GRA15490
GRA15500
GRA15510
GRA15520
GRA15530
GRA15540
GRA15550
GRA15560
GRA15570
GRA15580
GRA15590
GRA15600
GRA15610
GRA15620
GRA15630
GRA15640
GRA15650
GRA15660
GRA15670
GRA15680
GRA15690
GRA15700
GRA15710
GRA15720
GRA15730
GRA15740
GRA15750
GRA15760
GRA15770

```

100 ZMAX=HT
150 CONTINUE
    TMAC=ZMAX
    RETURN
END

C      SUBROUTINE STOCH(I,RANGE,A)
C
C      SUBROUTINE STOCH DETERMINES THE ATTRITION COEFFICIENTS WHEN
C      A USER HAS SELECTED A STOCHASTIC ATTRITION OPTION. THE CALCULATION
C      IS A FUNCTION OF THE ORIGINAL STOCHASTICALLY DETERMINED ATTRITION
C      COEFFICIENT AS WELL AS A FUNCTION OF RANGE.
C
COMMON /GRP6/ ALPHA(6)
COMMON /GRP3/ NBU,NRU,FL(6),FO(6),NOI(3),XIC(3,200),YIC(3,200),
1 IDIR(3,200),AVSP,ISPD
1 IUSTAT(6),I(6),LOST(6,6),VISFRA,VISFR8,SIZETK,
1 SIZETW,NT(6),NF(6),SRF,DISMAX,
1 INLOSC(6,6),VISFR(6,6),RMINTK,RMXTW,OP,TOWFR,TNKFR,
1 IPTT(3,3),RF,POA(6,6),APOA(6,6),LOA(6,6),NA(6),OFL(6),POL(6)
IF(I.EQ.2) GO TO 5003
A=ALPHA(I)*((1.0-RANGE/RMXTW)**2)
GO TO 5004
5003 A=ALPHA(I)*((1.0-RANGE/RMXTK)**2)
5004 RETURN
END

C      SUBROUTINE ETK(I,RANGE,T)
C
C      SUBROUTINE ETK COMPUTES THE EXPECTED TIME FOR A GIVEN FIRER TO
C      KILL A GIVEN TARGET. THE CALCULATION IS A FUNCTION OF RANGE,
C      TIME OF FLIGHT FOR A ROUND AND HIT AND KILL PROBABILITIES FOR
C      THE FIRING WEAPON SYSTEM. IT IS A NUMBER THAT IS USED IN THE
C      COMPUTATION OF THE DETERMINISTIC ATTRITION COEFFICIENTS.
C
COMMON /GRP2/ TA(2),TL(2),TH(2),TM(2),TF1(2),TF2(2),TF3(2),
1 P(2,6),PHH(2,6),PHM(2,6),PKH(2,6),TF(2)
IF(I.EQ.2) GOTO 5
TF(1)=TF1(I)
GOTO 6
5 IF(RANGE.GT.1000.0) GOTO 7
TF(1)=TF1(I)-(TF1(I)*((1000.0-RANGE)/1000.0))
GOTO 6
7 IF(RANGE.GT.2000.0) GOTO 8
TF(1)=TF2(I)-((TF2(I)-TF1(I))*((2000.0-RANGE)/1000.0))
GOTO 6
8 TF(1)=TF3(I)-((TF3(I)-TF2(I))*((3000.0-RANGE)/1000.0))
6 J=(RANGE+250.0)/500.0

```

GRA15780
GRA15790
GRA15800
GRA15810
GRA15820
GRA15830
GRA15840
GRA15850
GRA15860
GRA15870
GRA15880
GRA15890
GRA15900
GRA15910
GRA15920
GRA15930
GRA15940
GRA15950
GRA15960
GRA15970
GRA15980
GRA15990
GRA16000
GRA16010
GRA16020
GRA16030
GRA16040
GRA16050
GRA16060
GRA16070
GRA16080
GRA16090
GRA16100
GRA16110
GRA16120
GRA16130
GRA16140
GRA16150
GRA16160
GRA16170
GRA16180
GRA16190
GRA16200
GRA16210
GRA16220
GRA16230
GRA16240
GRA16250

```

IF(J.GT.6) J=6
T=TA(I)+TI(I)-TH(I)+((TH(I)+IF(I))/PKH(I,J))+((TM(I)+IF(I))/
1PHM(I,J))*((1.0-PH(I,J))/PKH(I,J)+PHH(I,J)-P(I,J))
RETURN
END
C SUBROUTINE SORT(I,M)
C
C SUBROUTINE SORT IS USED TO SORT TARGETS IN ASCENDING RANGE
C ORDER. THIS IS USED TO DETERMINE THE PRIORITY OF A TARGET
C FOR FIRE ALLOCATION.
C
COMMON /GRP5/ LOT(6,6),ROT(6,6)
DO 19 J=1,M
IF(ROT(I,M).GE.ROT(I,J)) GOTO 19
21 R=ROT(I,J)
NN=LOT(I,J)
RCT(I,J)=ROT(I,M)
LOT(I,J)=LOT(I,M)
RCT(I,M)=R
LOT(I,M)=NN
19 CONTINUE
END
C SUBROUTINE KOVER(ZO,IMACT,SIZET,ZI,S,HTS,ZS,VISFRT)
C
C SUBROUTINE KOVER DETERMINES WHAT PORTION OF A PARTICULAR TARGET
C IS COVERED BY THE TERRAIN BETWEEN THE TARGET AND OBSERVER.
C THIS NUMBER IS USED IN THE DETECTION AND ATTRITION COMPUTATION.
C
IF(S.EQ.0.) GO TO 2000
IF(HTS.GE.ZS) GO TO 2050
HEXT=ZO+(HTS-ZO)/S
EVIST=AMAX1(HEXT,IMACT)
IF(EVIST.GE.ZI) GO TO 2050
IF(EVIST.LE.ZI-SIZET) RETURN
VIS=(ZI-EVIST)/SIZET
IF(VIS.LT.VISFRT) VISFRT=VIS
RETURN
2000 IF(HTS.LT.ZO) RETURN
2050 VISFRT=0.0
RETURN
END
C SUBROUTINE LOS(XA,YA,TMACA,TMICA,SIZEA,XB,YB,TMACB,TMICB,SIZEB,
C -LATOB,LBTGA,VISFRA,VISFRB)

```

```

C SUBROUTINE LOS COMPUTES A PERCENT OF A TARGET VISIBLE TO A
C PARTICULAR OBSERVER, GIVEN THE COORDINATES OF BOTH.
COMMON /HILLS/ XC(100),YC(100),PEAK(100),ANGH(100),SPRD(100)
COMMON /HILLS/ ECC(100),PXX(100),PY(100),PXY(100),BASE
COMMON /HILLS/ NHILLS
COMMON /COVER/ CX(150),CYC(150),CPEAK(150),CPXX(150),CPYY(150)
COMMON /COVER/ CPXY(150),NCVELS
COMMON /COUNTR/KH,KHW,KV,KN,KGRS,KELL,KINT
COMMON /GRID/ LST(5,4),NHL(5,4),LISTH(150),KHREP(150),KTREP
COMMON /GRID/ LSTC(5,4),NC(5,4),LISTC(400),KCREP(150)
COMMON /GRID/ IGY(100),IEL(100),CSI(100),CS2(100)
DIMENSION IGX(100),IGY(100),IEL(100),CSI(100),CS2(100)
DATA GSIZE/1000./
C SUBROUTINE TO COMPUTE FRACTION VISIBLE FOR OBSERVER TARGET PAIRS
VISFRA=1.
VISFRB=1.
XBA=XB-XA
YBA=YB-YA
IF((XBA.EQ.0.).AND.(YBA.EQ.0.)) RETURN
IF(SIZEA+TMICB.LE.0.) GO TO 510
IF(SIZEB+TMICB.LE.0.) GO TO 510
IF(TMICA.LT.0.) VISFRA=1.0+TMICA/SIZEA
IF(TMICB.LT.0.) VISFRB=1.0+TMICB/SIZEB
ZA=TMACA + TMICA + SIZEA
ZB=TMACB + TMICB + SIZEB
KTREP=KTREP+1
ZBA=ZB-ZA
XBASQ=XBA*XBA
YBASQ=YBA*YBA
XYBA=XBA*YBA
TWOXBA=2.*XBA
TWOYBA=2.*YBA
NGRSQ=0
IF(XBA) 110,95,100
XBA=0.1
ISGX=-1
XINC=GSIZE/XBA
GO TO 120
ISGX=1
XINC=-GSIZE/XBA
IF(YBA) 140,125,130
YBA=0.1
ISGY=-1
YINC=GSIZE/YBA
GO TO 150
ISGY=1
YINC=-GSIZE/YBA
C COMPUTE GRID SQUARES CROSSED BY A TO B LINE
95 IF(XBA) 110,95,100
100 XBA=0.1
ISGX=-1
XINC=GSIZE/XBA
GO TO 120
110 ISGX=1
XINC=-GSIZE/XBA
IF(YBA) 140,125,130
120 YBA=0.1
ISGY=-1
YINC=GSIZE/YBA
GO TO 150
130 ISGY=1
YINC=-GSIZE/YBA
140

```

GRA16260
 GRA16270
 GRA16280
 GRA16290
 GRA16300
 GRA16310
 GRA16320
 GRA16330
 GRA16340
 GRA16350
 GRA16360
 GRA16370
 GRA16380
 GRA16390
 GRA16400
 GRA16410
 GRA16420
 GRA16430
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 GRA16450
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 GRA16470
 GRA16480
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 GRA16500
 GRA16510
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 GRA16580
 GRA16590
 GRA16600
 GRA16610
 GRA16620
 GRA16630
 GRA16640
 GRA16650
 GRA16660
 GRA16670
 GRA16680
 GRA16690
 GRA16700
 GRA16710
 GRA16720
 GRA16730

GRAI 6740
GRAI 6750
GRAI 6760
GRAI 6770
GRAI 6780
GRAI 6790
GRAI 6800
GRAI 6810
GRAI 6820
GRAI 6830
GRAI 6840
GRAI 6850
GRAI 6860
GRAI 6870
GRAI 6880
GRAI 6890
GRAI 6900
GRAI 6910
GRAI 6920
GRAI 6930
GRAI 6940
GRAI 6950
GRAI 6960
GRAI 6970
GRAI 6980
GRAI 6990
GRAI 7000
GRAI 7010
GRAI 7020
GRAI 7030
GRAI 7040
GRAI 7050
GRAI 7060
GRAI 7070
GRAI 7080
GRAI 7090
GRAI 7100
GRAI 7110
GRAI 7120
GRAI 7130
GRAI 7140
GRAI 7150
GRAI 7160
GRAI 7170
GRAI 7180
GRAI 7190
GRAI 7200
GRAI 7210

```

150  IX=1+IF IX(XB/GSIZE)
      IY=1+IF IX(YB/GSIZE)
      XNEXT=GSIZE*(FLOAT(IX)+0.5*(ISGX-1.))
      YNEXT=GSIZE*(FLOAT(IY)+0.5*(ISGY-1.))
      XSTEP=(XB-XNEXT)/XBA
      YSTEP=(YB-YNEXT)/YBA
      NGRSQ=NGRSQ+1
      IGY(NGRSQ)=IX
      IF((XSTEP.GT.1.) .AND. (YSTEP.GT.1.)) GO TO 200
      IF(XSTEP.YSTEP) 170,180,190
160  IX=IX + ISGX
      XSTEP=XSTEP+XINC
      GO TO 160
170  IX=IX+ISGX
      XSTEP=XSTEP+XINC
180  IY=IY+ISGY
      YSTEP=YSTEP+YINC
      GO TO 160
190  KGRS=KGRS+NGRSQ
200  C GRID SQUARE LIST NOW COMPLETE IN IGX, IGY WITH NGRSQ ENTRIES
      C
      C NOW FIND WHICH COVER ELLIPSES TOUCH THE A TO B LINE,
      C CHECK ELEVATIONS AT S1 AND S2 FOR EACH SUCH ELLIPSE
      NELS=0
      CHTMAX=0
      IF(NCVELS.EQ.0) GOTO 270
      DO 260 K=1,NGRSQ
      IX=IGX(K)
      IY=IGY(K)
      N=NC(IX,IY)
      IF(N.EQ.0) GO TO 260
      LS=LSTC(IX,IY)
      LEND=LS+N-1
      DO 250 L=LS,LEND
      KELL=KELL+1
      IC=LISTC(L)
      IF(KCREP(IC).EQ.KTREP) GO TO 250
      KCREP(IC)=KTREP
      RX=XA-CXC(IC)
      RY=YA-CYC(IC)
      PPXX=CPXX(IC)
      PPYY=CPYY(IC)
      PPXY=CPXY(IC)
      AA=PPXX*XBASQ+PPYY*YBASQ+PPXY*XYBA
      BB=PPXX*TWDXBA*RX+PPYY*TWDYBA*RY+PPXY*(RX*YBA+RY*XBA)
      CC=PPXX*RX*RX+PPYY*RY*RY+PPXY*RX*RY-1.0
      ARG=BB*BB-4.0*AA*CC

```

GRA17220
 GRA17230
 GRA17240
 GRA17250
 GRA17260
 GRA17270
 GRA17280
 GRA17290
 GRA17300
 GRA17310
 GRA17320
 GRA17330
 GRA17340
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 GRA17610
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 GRA17630
 GRA17640
 GRA17650
 GRA17660
 GRA17670
 GRA17680
 GRA17690

```

IF(ARG.LE.0.) GO TO 250
SQ=SQR7(ARG)
S1=-(BB+SQ)/(2.0*AA)
S2=(SQ-BB)/(2.0*AA)
IF(S1.GE.1.) GO TO 250
IF(S2.LE.0.) GO TO 250
IF(S1.LE.0.) GO TO 510
IF(S2.GE.1.) GO TO 510
CHECK LOS AT S1 AND S2
C NOW KINT=KINT+1
CPK=CPEAK(IC)
XS=XA+S2*XBA
YS=YA+S2*YBA
CALL ELEV(XS,YS,HTS)
HTS=HTS+CPK
ZS=ZA+S2*ZBA
IF(LATOB.EQ.0) GO TO 210
CALL KOVER(ZA,TMACB,SIZEB,ZB,S2,HTS,ZS,VISFRB)
IF(VISFRB.LE.0.) GO TO 510
IF(LBTQA.EQ.0) GO TO 220
S=1.-S2
CALL KOVER(ZB,TMACA,SIZEA,ZA,S,HTS,ZS,VISFRA)
IF(VISFRA.LE.0.) GO TO 510
XS=XA+S1*XBA
YS=YA+S1*YBA
CALL ELEV(XS,YS,HTS)
HTS=HTS+CPK
ZS=ZA+S1*ZBA
IF(LATOB.EQ.0) GO TO 230
CALL KOVER(ZA,TMACB,SIZEB,ZB,S1,HTS,ZS,VISFRB)
IF(VISFRB.LE.0.) GO TO 510
IF(LBTQA.EQ.0) GO TO 240
S=1.0-S1
CALL KOVER(ZB,TMACA,SIZEA,ZA,S,HTS,ZS,VISFRA)
IF(VISFRA.LE.0.) GO TO 510
NELS=NELS+1
TEL(NELS)=IC
CS1(NELS)=S1
CS2(NELS)=S2
IF(CPK.GT.CHTMAX) CHTMAX=CPK
CONTINUE
CONTINUE
C ALL ELLIPSES CHECKED
250
260
C NOW START ON THE HILLS
270 DO 600 K=1,NGRSQ
    IX=IGX(K)
    IY=IGY(K)
  
```

GRA17700
 GRA17710
 GRA17720
 GRA17730
 GRA17740
 GRA17750
 GRA17760
 GRA17770
 GRA17780
 GRA17790
 GRA17800
 GRA17810
 GRA17820
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 GRA17980
 GRA17990
 GRA18000
 GRA18010
 GRA18020
 GRA18030
 GRA18040
 GRA18050
 GRA18060
 GRA18070
 GRA18080
 GRA18090
 GRA18100
 GRA18110
 GRA18120
 GRA18130
 GRA18140
 GRA18150
 GRA18160
 GRA18170

```

IF(NHL(IX,IY).EQ.0) GO TO 600
LS=LST(IX,IY)
LEND=LS+NHL(IX,IY)-1
DO 500 L=LS,LEND
  I=LISTH(L)
  IF(KHREP(I).EQ.KTREP) GO TO 500
  KHREP(I)=KTREP
  C PROCESSING FOR HILL I STARTS HERE
  KH=KH+1
  C COMPUTE W = TOP OF THIS HILL ALONG O-T LINE
  C
  TRX=XA-XC(I)
  TRY=YA-YC(I)
  TPXX=PX(X(I))
  TPYY=PY(Y(I))
  TPXY=PX(Y(I))
  FQ=TPXX*TRX+TPYY*TRY+TPXY*(TRX*YB+TRY*XBA)
  GQ=TPXX*XBASQ+TPYY*YBASQ+TPXY*XYBA
  IF(GQ.EQ.0.) GO TO 500
  W=-FQ/(2.*GQ)
  IF(ABS(W).GT.5.) GO TO 500
  FSQ=FQ*FQ
  EQ=TPXX*TRX+TPYY*TRY+TPXY*TRX*TRY
  C
  POWER=EQ-FSQ/(4.*GQ)
  IF(POWER.LT.-3.) GO TO 500
  HHW=PEAK(I)*EXP(POWER)
  KHW=KHW+1
  IF(HHW.LE.BASE) GO TO 500
  ZW=ZA+W*ZBA
  IF((W.LT.0.)OR.(W.GT.1.)) GO TO 300
  IF(HHW.GE.ZW) GO TO 510
  CVHTW=0.
  IF(NELS.EQ.0) GO TO 300
  DO 280 M=1,NELS
    IF((CS1(M).GE.W).OR.(CS2(M).LE.W)) GO TO 280
    IC=ICEL(M)
    IF(CVHTW.LT.CPEAK(IC)) CVHTW=CPEAK(IC)
  280 CONTINUE
  IF((HHW+CVHTW).GE.ZW) GO TO 510
  300 IF(HHW+CHTMAX.LT.AMIN1(ZA-SIZEA,ZB-SIZEB)) GO TO 500
  C IF WE GET TO HERE THEN NEED TO FIND LOWEST SIGHT LINE OVER HILL
  C NEWTON ITERATION A TO B GIVING VISFRB
  IF(LATOB.EQ.0) GO TO 400
  KV=KV+1
  V=W
  HHV=HHW
  NCT=0
  
```


GRA18180
GRA18190
GRA18200
GRA18210
GRA18220
GRA18230
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GRA18250
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GRA18290
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GRA18310
GRA18320
GRA18330
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GRA18560
GRA18570
GRA18580
GRA18590
GRA18600
GRA18610
GRA18620
GRA18630
GRA18640
GRA18650

```

330      FV=FQ*V
          TWOGV=2.*GQ*V
          FCNV=ZA+HHV*(TWOGV*V+V-1.)
          KN=KN+1
          FACTOR=(TWOGV*TWOGV+2.*(GQ+TWOGV*FQ)+FSQ)
          DFCNV=HHV*V*FACTOR
          IF (ABS(DFCNV) .LT. 1.E-10) GO TO 350
          V=V-FCNV/DFCNV
          FV=FQ*V
          TWOGV=2.*GQ*V
          POWER = EQ+V+GQ*V*V
          IF (POWER .LT. -3.) GO TO 400
          HHV=PEAK(I)*EXP(POWER)
          DHHV=HHV*(FQ+TWOGV)
          ELV=ZA+DHHV*V
          IF (ABS(HHV-ELV) .LT. 1.) GO TO 350
          NCT=NCT+1
          IF (NCT.LT.10) GO TO 330
          IF ((V.LT.0.)OR.(V.GT.1.)) GO TO 400
          CVHTV=0.
          IF (NELS.EQ.0) GO TO 390
          DO 380 M=1,NELS
          IF ((CS1(M).GE.V).OR.(CS2(M).LE.V))GO TO 380
          IC=IEL(M)
          IF (CVHTV.LT.CPEAK(IC)) CVHTV=CPEAK(IC)
          CONTINUE
          HTV=HHV+CVHTV
          ZV=ZA+V*ZBA
          CALL KOVER(ZA,TMACB,SIZEB,ZB,V,HTV,ZV,VISFRB)
          IF (VISFRB.LE.0.) GO TO 510
          C NEWTON ITERATION 8 TO A GIVING VISFRA
          IF (ABS(V).GT.5.)GO TO 400
          IF (LBTOA.EQ.0) GO TO 500
          KV=KV+1
          V=W
          VM1=V-1.
          HHV=HHW
          NCT=0
          FV=FQ*V
          TWOGV=2.*GQ*V
          FCNV=ZB+HHV*((FQ+TWOGV)*VM1-1.)
          KN=KN+1
          FACTOR=(TWOGV*TWOGV+2.*(GQ+TWOGV*FQ)+FSQ)
          DFCNV=HHV*VM1*FACTOR
          IF (ABS(DFCNV) .LT. 1.E-10) GO TO 450
          V=V-FCNV/DFCNV
          IF (ABS(V).GT.5.)GO TO 500
          VM1=V-1.
400
430

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GRA18660
GRA18670
GRA18680
GRA18690
GRA18700
GRA18710
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GRA18870
GRA18880
GRA18890
GRA18900
GRA18910
GRA18920
GRA18930
GRA18940
GRA18950

```

FV=FQ*V
TWOGV=2.*GQ*V
POWER = EQ+FV+GQ*V*V
IF(POWER.LT.-3.) GO TO 500
HHV=PEAK(I)*EXP(POWER)
DHV=HHV*(FQ+TWOGV)
ELV=ZB+DHV*VM1
IF (ABS(HHV-ELV) .LT.1.) GO TO 450
NCT=NCT+1
IF (NCT.LT.10) GO TO 430
IF ((V.LT.0.).OR.(V.GT.1.)) GO TO 500
CVHTV=0.
IF (NELS.EQ.0) GO TO 490
DO 480 M=1,NELS
  IC=ICEL(M)
  IF ((CS1(M).GE.V).OR.(CS2(M).LE.V)) GO TO 480
  IF (CVHTV.LT.CPEAK(IC)) CVHTV=CPEAK(IC)
CONTINUE
HTV=HHV+CVHTV
ZV=ZA+V*ZBA
S=-VM1
CALL KOVER(ZB,TM,CA,SIZEA,ZA,S,HTV,ZV,VISFRA)
IF (VISFRA.LE.0.) GO TO 510
CONTINUE
CONTINUE
RETURN
VISFRA=0.
VISFRB=0.
RETURN
END

```

450

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490

500
600

510

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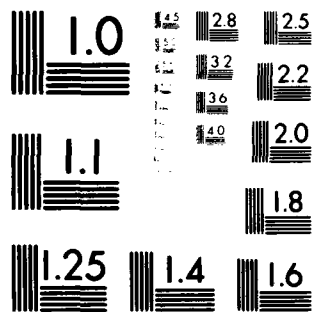
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MICROCOPY RESOLUTION TEST CHART
NATIONAL BUREAU OF STANDARDS-1963-A

PLOTTING PROGRAM FOR TERRAIN CONTOUR LINE

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      IF(ZVAL.GT.140.) GO TO 189
      IF(ZVAL.NE.20.AND.ZVAL.LT.100.) GO TO 189
      XXH(ME)=XEL
      YYH(ME)=YEL
      ME=ME+1
189  NVAL1=KVAL
      YEL=YRES
      GO TO 727
333  NP=ME-1
      CALL PLOTG(XXH,YYH,NP,1,0,75,'X-AXIS LABEL',12,
1      'Y-AXIS LABEL',12,XMIN,XMAX,YMIN,YMAX,8.,6.)
      CALL PLOT(0.,0.,999)
      STOP
      END
      SUBROUTINE ELEV(X,Y,TMAC)

```

C
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COMPUTE THE ELEVATION FOR A GIVEN X,Y COORDINATE

```

      IMPLICIT REAL*4(A-H,O-Z)
      COMMON /HILLS/ XC(100),YC(100),PEAK(100),ANGH(100)
      COMMON /HILLS/ SPRO(100),ECC(100),PXX(100),PYY(100)
      COMMON /HILLS/ PXY(100),BASE,NHILLS
      COMMON /GRID/ LST(5,4),NHL(5,4),LISTH(100),KHREP(100)
      COMMON /GRID/ KTREP
      DATA GSIZE/1000./
      ZMAX=BASE
      IX=1+IFIX(X/GSIZE)
      IY=1+IFIX(Y/GSIZE)
      IF(NHL(IX,IY).EQ.0) GO TO 150
      LS=LST(IX,IY)
      LEND=LS+NHL(IX,IY)-1
      DO 100 L=LS,LEND
      I=LISTH(L)
      QX=X-XC(I)
      QY=Y-YC(I)
      QXSQ=QX*QX
      QYSQ=QY*QY
      QXY=QX*QY
      FACTOR=PXX(I)*QXSQ+PYY(I)*QYSQ+PXY(I)*QXY
      IF(FACTOR.LT.-3.) GO TO 100
      HT=PEAK(I)*EXP(FACTOR)
      IF(HT.LE.ZMAX) GO TO 100
      ZMAX=HT
100  CONTINUE
150  TMAC=ZMAX
      RETURN
      END

```

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